

**GUGGENHEIM AERONAUTICAL LABORATORY**

**CALIFORNIA INSTITUTE OF TECHNOLOGY**

AN APPLICATION OF THE METHOD OF CHARACTERISTICS  
TO AXIALLY SYMMETRIC SUPERSONIC FLOW

THESIS BY

Lt. Comdr. C. W. Griffing, USN  
Lt. Comdr. W. C. Wilburn, USN  
Lt. Comdr. D. Pardon, USN  
Lt. Comdr. E. W. McLaughlin, USN

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Lt. Comdr. C. W. Griffing, U.S.N.  
Lt. Comdr. W. C. Wilburn, U.S.N.  
Lt. Comdr. D. Purdon, U.S.N.  
Lt. Comdr. E. W. McLaughlin, U.S.N.

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## INTRODUCTION

The method of characteristics for three dimensional axially symmetric bodies was used to determine the velocity distribution about the nose of the Corporal E rocket, a rocket projectile, for Mach numbers 2 and 4. From the velocities the pressure distribution was determined and a drag coefficient computed.

For a starting point the nose of the projectile was approximated for a short distance by a cone and the Taylor-Maccoll<sup>\*</sup> solution to this problem was used. This solution gave the angle of shockwave and the body. The Sauer graphical-numerical iteration method was used for the remainder of the solution.

Preliminary calculations and the work for Mach number 3 were carried out by Dr. H. K. Forster to whom we are indebted for instruction and aid with this work.

<sup>\*</sup>Taylor, G. I. and Maccoll, J. W., Proc. Roy. Soc., A, Vol. 139, pp 278-311 1933.

## CHARACTERISTICS\*

The following discussion is for two dimensional flow and is taken from "Introduction to Aerodynamics of a Compressible Fluid", by H. W. Liepmann and Allen E. Puckett.

The term "characteristic" is related by definition to properties of certain partial differential equations. For any second order, partial differential equation of the type

$$(1) \quad A \frac{\partial^2 Z}{\partial x^2} + 2B \frac{\partial^2 Z}{\partial x \partial y} + C \frac{\partial^2 Z}{\partial y^2} = D \frac{\partial Z}{\partial x} + E \frac{\partial Z}{\partial y} + \dots$$

two families of curves may be defined by the total differential equations

$$(2) \quad \frac{dy}{dx} = \frac{B \pm \sqrt{B^2 - AC}}{A}$$

where A, B, and C are functions of x and y. These curves (2) are known as the characteristics of equation (1).

These characteristics have certain properties which make them useful in an approximate solution process. These properties will be listed without proof:

1) They are invariant under transformation.

2) A solution  $Z(x,y)$  to equation (1) may be composed of separate integral surfaces joining continuously with continuous derivatives along a line. This line is a characteristic. This property of the branching of integral surfaces along a characteristic permits us to regard the line as a wave front along which a disturbance is propagated through a field.

\*Liepmann, H. W. and Puckett, Allen E. Introduction to Aerodynamics of a Compressible Fluid. pp 229-232 1947

3) Boundary conditions along any line,  $C$ , in the field will define a solution within a triangle bounded by  $C$  and the characteristics through the end points of  $C$ . Boundary conditions along a characteristic, however, will not define a solution in any region; boundary conditions must be given along two intersecting characteristics of different families. The exact equation of the velocity potential is:

$$(3) (a^2 - u^2) \frac{\partial^2 \phi}{\partial x^2} - 2uv \frac{\partial^2 \phi}{\partial x \partial y} + (a^2 - v^2) \frac{\partial^2 \phi}{\partial y^2} = 0$$

where  $u = \frac{\partial \phi}{\partial x}$        $v = \frac{\partial \phi}{\partial y}$

If a new dependent variable is defined

$$F(u, v) = ux + vy - \phi$$

then when a transformation is made to the hodograph plane, an element of the  $F$  surface in the  $(u, v)$  plane is defined by an element of the  $(x, y)$  surface. (Legendre Transformation). The transformation of equation (3) becomes

$$(4) (a^2 - v^2) F_{uu} + 2uv F_{uv} + (a^2 - u^2) F_{vv} = 0$$

The characteristics of the equation are

$$(5) \frac{dv}{du} = \frac{uv \pm \sqrt{u^2 v^2 - (a^2 - u^2)(a^2 - v^2)}}{(a^2 - v^2)}$$

This equation can be integrated immediately, "a" having been expressed as a function of  $u$  and  $v$ . Thus in the two dimensional case a characteristic chart may be constructed and is known as the "Prandtl-Busemann Characteristic Diagram."

When an attempt is made to use this method in three dimensional problems it is found that it cannot be done. A Legendre Transformation



leads to a non-linear equation in this case. In general, in three dimensional flow, it is not possible to construct a characteristic diagram. Instead, a separate construction must be carried out for each flow.

## SAUER METHOD

The Sauer solution of supersonic axially symmetric flow is a graphical-numerical iteration method.

For a non-viscous, steady, isentropic flow of a perfect fluid without body forces, the equation of motion may be obtained by eliminating the pressure and density from the force equations and the equation of continuity. Transformed to cylindrical coordinates, and assuming axial symmetry, this becomes

$$(6) \left(1 - \frac{u^2}{a^2}\right) \frac{\partial u}{\partial x} + \left(1 - \frac{v^2}{a^2}\right) \frac{\partial v}{\partial r} - uv \left(\frac{\partial u}{\partial r} + \frac{\partial v}{\partial x}\right) + \frac{v}{r} = 0$$

Assuming irrotational flow the velocity components may be replaced by the proper derivatives of the velocity potential  $\phi$ .

In the axially symmetric case, given a velocity vector,  $V$ , one can introduce in an axial plane a set of <sup>orthogonal</sup> axes in which  $X'$  is along the velocity vector. Then  $u' = V$  and  $v' = 0$  where  $u'$  is the velocity in the  $X'$  direction and  $v'$  is the velocity in the  $Y'$  direction.

If at a particular point the  $X'$ ,  $Y'$  coordinates are introduced equation (6) becomes

$$\left(1 - \frac{u'^2}{a^2}\right) \frac{\partial u'}{\partial x'} + \frac{\partial v'}{\partial y'} + \frac{v'}{r} = 0$$

and introducing  $\phi$ , for irrotational flow

$$(7) \left(1 - \frac{V^2}{a^2}\right) \frac{\partial^2 \phi}{\partial x'^2} + \frac{\partial^2 \phi}{\partial y'^2} + \frac{1}{r} \frac{\partial \phi}{\partial r} = 0$$

The Mach angle is defined as  $\alpha = \sin^{-1} \frac{v}{a}$  where  $a$  is the local speed of sound and  $V$  the local fluid velocity. A Mach line is a line inclined to the direction of fluid flow by an angle equal to the Mach angle.

At a point, where the velocity is known two Mach lines may be drawn. In this case where the velocity is along the  $X'$  axis, one Mach line will be at an angle and one at an angle from the  $X'$  axis. (See Fig. 1 a).

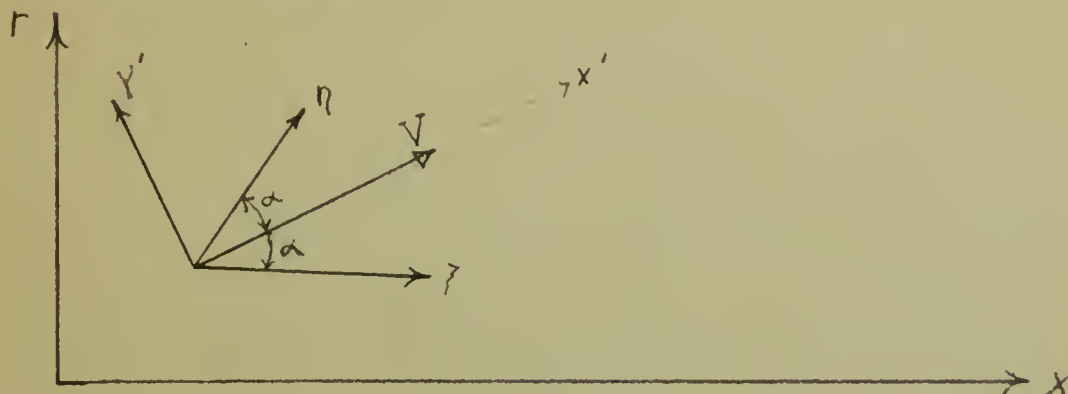


Fig. (1) a

These Mach lines, which may be identified as the characteristics of equation (6) define a new set of coordinate axes, and .

From the definition of the Mach angle,  $\sin$  it is seen that substituting this in equation (7) we get

$$(8) \quad \cot^2 \alpha \frac{\partial^2 \phi}{\partial X'^2} - \frac{\partial^2 \phi}{\partial Y'^2} = \frac{1}{\lambda} \frac{\partial \phi}{\partial \lambda}$$

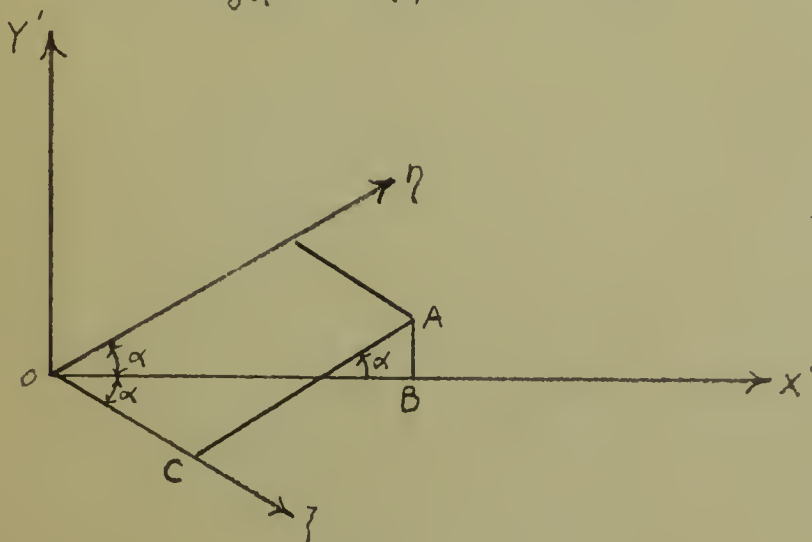


Fig. (1) b

$$\left. \begin{aligned} \overline{OB} = x' &= \overline{OC} \cos \alpha + \overline{CA} \cos \alpha = (\zeta + \eta) \cos \alpha \\ \overline{AB} = y' &= -\overline{OC} \sin \alpha + \overline{CA} \sin \alpha = (-\zeta + \eta) \sin \alpha \end{aligned} \right\} \text{From Fig. 1(b)}$$

$$\text{Hence: } \zeta = \frac{1}{\sin 2\alpha} (x' \sin \alpha - y' \cos \alpha)$$

$$\eta = \frac{1}{\sin 2\alpha} (x' \sin \alpha + y' \cos \alpha)$$

$$\frac{\partial \phi}{\partial x'} = \frac{\partial \phi}{\partial \zeta} \frac{\partial \zeta}{\partial x'} + \frac{\partial \phi}{\partial \eta} \frac{\partial \eta}{\partial x'} = \frac{1}{\sin 2\alpha} \left( \sin \alpha \frac{\partial \phi}{\partial \zeta} + \sin \alpha \frac{\partial \phi}{\partial \eta} \right) = \frac{1}{2 \cos \alpha} \left( \frac{\partial \phi}{\partial \zeta} + \frac{\partial \phi}{\partial \eta} \right)$$

$$\frac{\partial \phi}{\partial y'} = \frac{\partial \phi}{\partial \zeta} \frac{\partial \zeta}{\partial y'} + \frac{\partial \phi}{\partial \eta} \frac{\partial \eta}{\partial y'} = \frac{1}{\sin 2\alpha} \left( -\cos \alpha \frac{\partial \phi}{\partial \zeta} + \cos \alpha \frac{\partial \phi}{\partial \eta} \right) = \frac{1}{2 \sin \alpha} \left( -\frac{\partial \phi}{\partial \zeta} + \frac{\partial \phi}{\partial \eta} \right)$$

$$\frac{\partial^2 \phi}{\partial x'^2} = \frac{1}{4 \cos^2 \alpha} \left( \frac{\partial^2 \phi}{\partial \zeta^2} + \frac{\partial^2 \phi}{\partial \eta^2} + 2 \frac{\partial^2 \phi}{\partial \zeta \partial \eta} \right)$$

$$\frac{\partial^2 \phi}{\partial y'^2} = \frac{1}{4 \cos^2 \alpha} \left( \frac{\partial^2 \phi}{\partial \zeta^2} + \frac{\partial^2 \phi}{\partial \eta^2} - 2 \frac{\partial^2 \phi}{\partial \zeta \partial \eta} \right)$$

substituting these relations in (8)

$$\frac{\partial^2 \phi}{\partial \eta \partial \zeta} = \frac{\sin^2 \alpha}{r} \frac{\partial \phi}{\partial r}$$

This equation can be written

$$(9) \quad \frac{d}{d\zeta} \left( \frac{\partial \phi}{\partial \eta} \right) = \frac{dq}{d\zeta} = \frac{\sin^2 \alpha}{r} v$$

$$\frac{d}{d\eta} \left( \frac{\partial \phi}{\partial \zeta} \right) = \frac{dp}{d\eta} = \frac{\sin^2 \alpha}{r} v$$

where p and q indicate the projections of the velocity vector along the  $\zeta$  and  $\eta$  directions respectively.

Replacing the derivatives of (9) by a quotient of increments

and clearing fractions the equations become

$$(10) \quad \begin{aligned} dq &= \frac{v}{r} \sin^2 \alpha d\zeta \\ dp &= \frac{v}{r} \sin^2 \alpha d\eta \end{aligned}$$

and  $d\zeta$  and  $d\eta$  being the increments in the directions of the Mach lines

and  $dp$  and  $dq$  the projections of the velocity increment upon the

Mach lines.



## PROCEDURE

The properties of the characteristics enable us to make an approximate solution. The mechanical process is a simultaneous construction of velocities in the hodograph plane and of Mach lines in the physical plane. Step by step small areas in the physical plane correspond to points in the hodograph plane since the flow field in the physical plane is divided into a finite number of small regions bounded by Mach lines over which averages are taken for computing velocities in the hodograph plane. Hence the accuracy of the computation will depend on the size of the regions bounded by Mach lines. The boundary conditions in the physical plane determine the direction of the velocity in the hodograph plane; at the shock wave the magnitude is also determined. The points in the hodograph plane when found by an iteration process based on estimates will in turn determine the Mach lines in the physical plane.

The two boundaries which define the boundary conditions are the shock wave attached to the nose and the surface of the body. Between these boundaries a net of Mach lines is constructed by proceeding from point to point until, in the entire area about the body and at points along the surface, the velocities are determined. This Mach net is shown in Fig. (5), Fig. (6) or Fig. (7).

The angle of the shock wave at the nose is obtained from Taylor-Maccoll solution of flow about a cone with the same nose angle. For this purpose, depending upon the geometry of the body the assumption that the nose is conical will be good at least a

small distance back from the vertex. Taylor and Maccoll showed that velocity magnitudes and directions are constant in supersonic flow about a cone along radial lines through the vertex. This solution furnishes as many points as needed to start the characteristic method solution. These points can be taken close enough to the vertex to make the conical flow assumption valid.

With the boundaries established and some points in the physical plane for which the velocities are known one may proceed by using the Sauer graphical method for computing supersonic axially symmetric flow. There are three different geometrical cases for which slightly different procedures are necessary. The cases are:

(a) from the known solution in two points in the free stream to calculate the solution in a third point in free stream;

(b) from the known solution in a point in the free stream to calculate the solution in a point on the body;

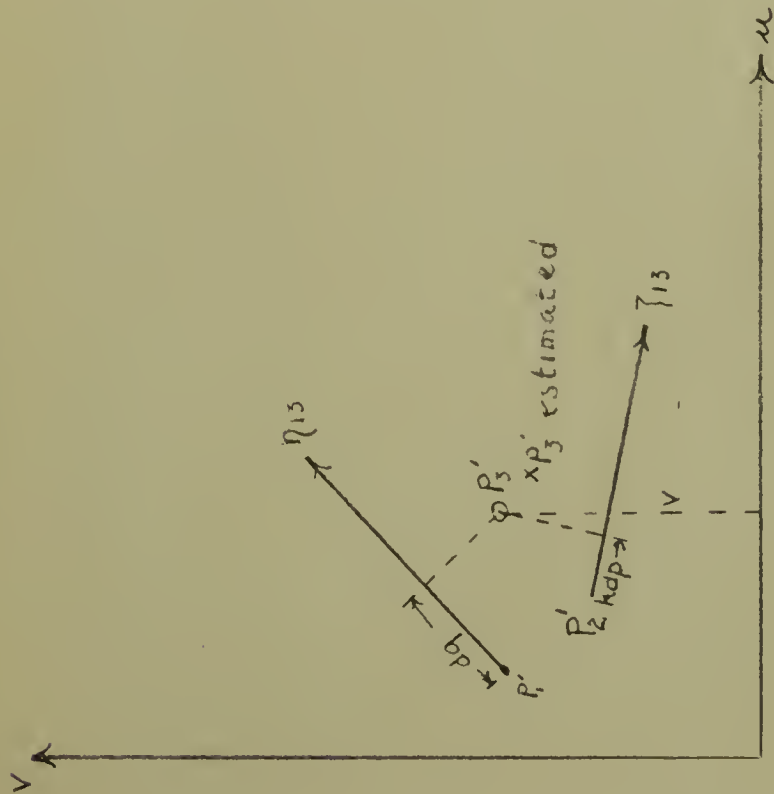
(c) from the known solution of a point on the shock wave and a point in the free stream to calculate the solution in a third point on the shock wave.

First, take the case of all points in the free stream. (see Fig. 2). Suppose points  $P_1$  and  $P_2$  are known: to find  $P_3$ ,  $P'_3$  is estimated in the hodograph plane. Then with mean values, magnitude and direction, which are estimated, draw an average  $\zeta_{13}$  and  $\eta_{23}$  line. Their intersection gives  $P_3$  in the physical plane from which values are obtained for  $d\zeta$ ,  $d\eta$  and  $\alpha$ . With these values one can calculate  $dq$  and  $dp$  from

$$dq = \sin^2 \alpha \frac{V}{\lambda} d\zeta$$

$$dp = \sin^2 \alpha \frac{V}{\lambda} d\eta$$

Hodograph plane



Physical Plane

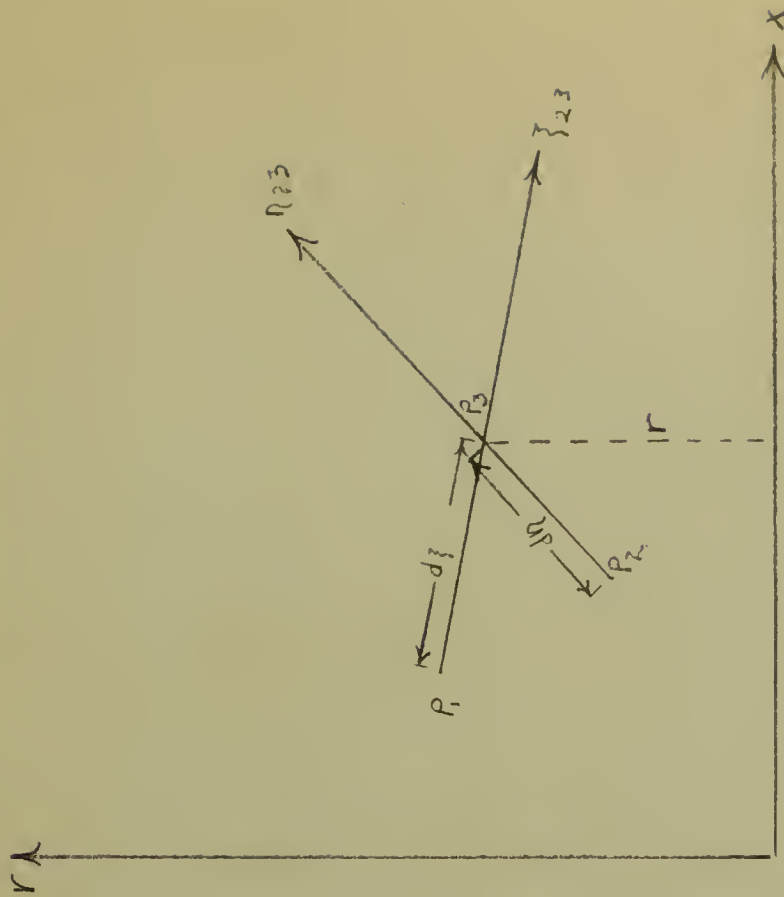


Fig. (2)



before. The velocities from successive points along the body fall, however, in a smooth curve in the hodograph plane making estimation easy with the result that the process generally does not need to be repeated.

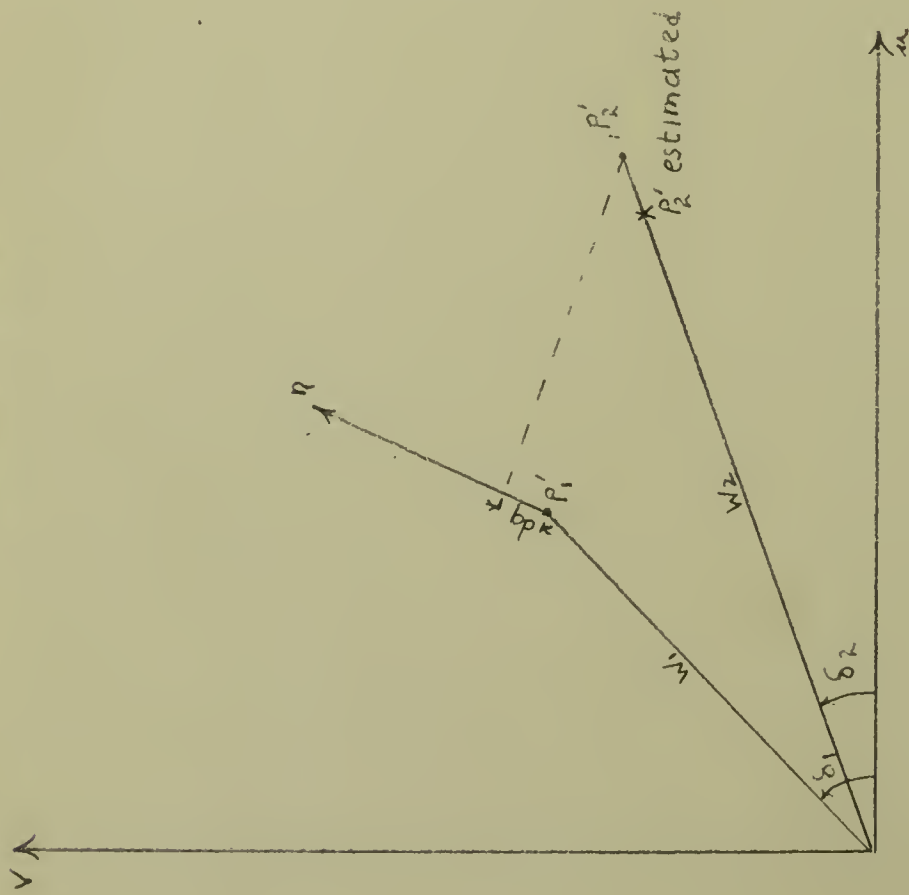
Now in obtaining a point on the shock wave from a preceding point on the shock wave and a point in the free stream it must be noted that the angle of the shock wave is not known. The shock wave is conical only for flow about a cone. For a curved profile the shock wave is also a curve which for this method is approximated by a series of straight lines, the angles of which must be found. To do this the Busemann shock polar is used in the hodograph plane. The shock polar graphically expresses the relation between the velocity direction and magnitude of the downstream flow and the angle of the shock wave for a given free stream velocity. Referring to Fig. (4) suppose  $P_1$  and  $P_2$  are known;  $P_3$  is to be found. Since  $P_3$  is on the shock wave it is also on the shock polar along with  $P_1'$  which is known. Estimate  $P_3'$  on the shock polar. The angle of the shock wave in the physical plane is the complement of the mean of  $\angle OAP_1$  and  $\angle OAP_3$ . The  $\eta$  line  $P_2P_3$  is obtained as in the free stream case. The intersection of this  $\eta$  line with the shock wave gives the values necessary to calculate  $dp$ . The construction in the hodograph plane is made giving the point  $P_3'$  at the intersection of the shock polar with the perpendicular to the  $\xi$  line from  $P_2'$ . Since the shock wave and the  $\eta$  line from  $P_2$  are nearly parallel it is often necessary to repeat the procedure.



Then stepping off  $dq$  in the  $\eta_{13}$  direction and  $dp$  in the  $\zeta_{23}$  direction perpendiculars are erected as shown in Fig. (2). These intersect in a point which will be very close or right on the estimated  $P_3'$ . If this is not within the desired accuracy the process is repeated until the iteration shows no change. Table I shows several examples of calculations made in obtaining the values necessary to construct Fig. (2).

For the case of obtaining a point on the surface of the body from a point in the free stream the procedure differs slightly. Referring to Fig. (3) suppose  $P_1$  is known;  $P_2$  is to be found. A  $\zeta$  line, whose direction is estimated, is drawn from  $P_1$  until it intersects the boundary at B. Since the flow is tangent to the boundary at all points on the boundary the direction of the flow velocity at point B is known, and an estimate of the magnitude of the flow velocity is made. From the mean between this estimated velocity and the velocity at  $P_1$  a Mach angle is calculated. Similarly a mean value of the angle of flow direction (between  $P_1$  and point B on the surface) is calculated. The difference between these two angles gives a new  $\zeta$  line intersecting the boundary at  ${}_1P_2$ . The points  $P_1$  and  ${}_1P_2$  give the values necessary to calculate  $dq$  as in the free stream case. As before the construction is made in the hodograph plane and the perpendicular at a distance  $dq$  from  $P_1'$  along the  $\eta$  line intersects  $w_2$  at  ${}_1P_2'$ . From the mean values of  $P_1'$  and  ${}_1P_2'$  draw the corresponding  $\zeta$  line from  $P_1$  in the physical plane. This should intersect the boundary at  ${}_1P_2$ . If not, one takes the tangent to the boundary at the new point and proceeds as

Hodograph Plane



Physical Plane

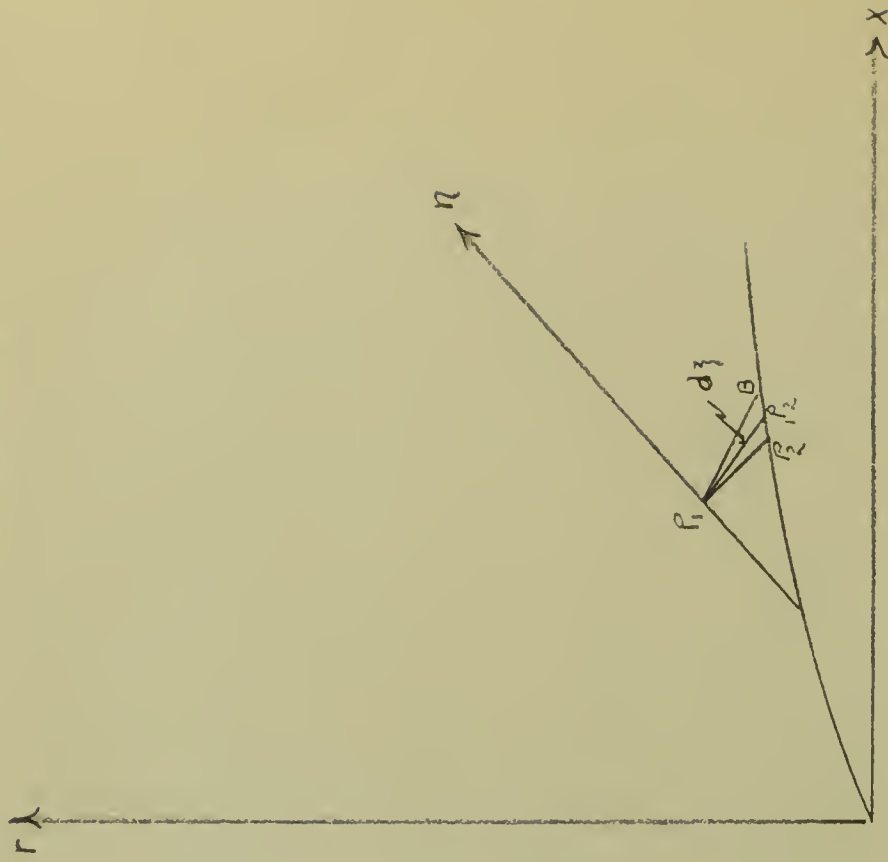


Fig. (3)

Hodograph plane



Physical Plane

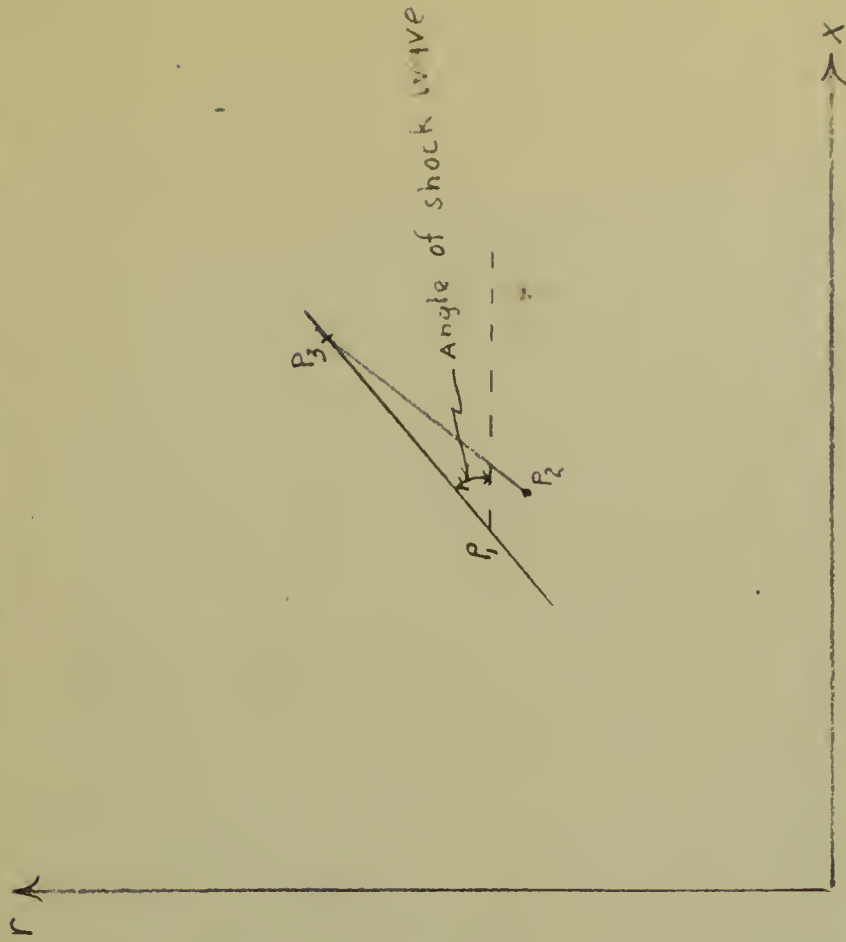
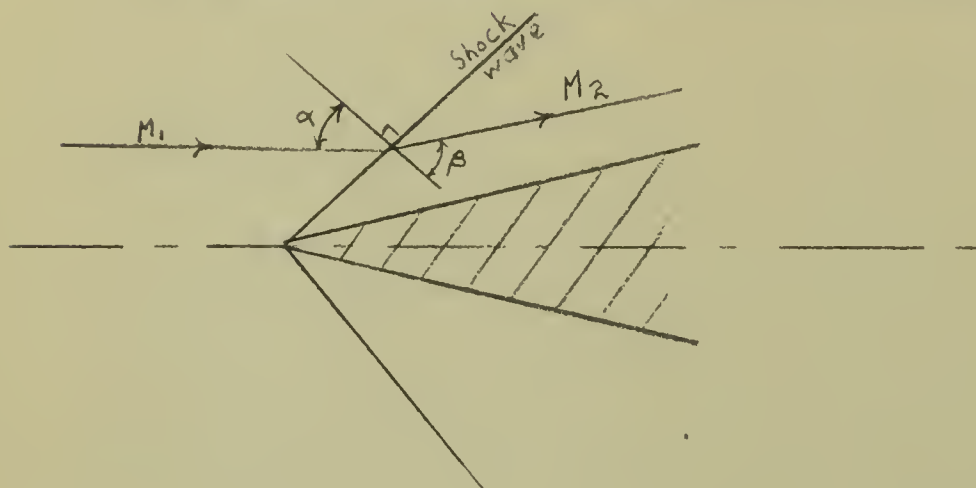


Fig. (4)

Then, 
$$C_p = Z \frac{\frac{p_2}{p_0} - \frac{p_1}{p_0}}{\frac{\gamma M_1^2}{2} \frac{p_1}{p_0}}$$

$Z$  is a function of the strength of the shock wave and thus of the shock wave angle, which is known from the Taylor-Maccoll solution (the angle of the shock wave is taken at the nose), and of the free stream Mach number.

Given  $M_1$  and  $\alpha$  (see figure below)  $Z$  is computed as follows\*:



$$1. \quad M_1^2 = \frac{2}{\gamma-1} \left[ \left( \frac{1}{\gamma} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]$$

$$2. \quad \cos^2 \alpha = \frac{[(\gamma-1) + (\gamma+1)\left(\frac{\gamma}{\gamma}\right)](\gamma-1)}{4\gamma \left[ \left( \frac{1}{\gamma} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]}$$

$$3. \quad \frac{\tan \beta}{\tan \alpha} = \frac{(\gamma-1) + (\gamma+1)\left(\frac{\gamma}{\gamma}\right)}{(\gamma+1) + (\gamma-1)\left(\frac{\gamma}{\gamma}\right)}$$

\*Durand, W. F., Aerodynamic Theory, Volume III, Durand Reprint, 1943, pp 238-240.

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# CALCULATION OF $C_p$ AND $C_D$

After the calculation of the flow velocities is completed, all of the points of the Mach net between the shock wave and the surface of the body are tabulated, i.e., the geometrical position of the point and the stream velocity at the point. (see Table II). In the calculation of the drag of the nose section, however, only the points on the surface of the missile are needed. Given a number of points on the surface and the velocities at these points the pressure coefficient,  $C_p$ , is computed for each of these points and a plot is made of  $C_p$  vs.  $X$ . (see Fig. (8)). From this curve values of  $C_p$  are obtained for regular increments of  $X$  and then by carrying out the appropriate integration (in this case a graphical integration was used; see Fig. (10)) the drag coefficient,  $C_D$ , can be obtained for the nose of the missile.

The equations used in the actual computations are discussed below:

In general

$$C_p = \frac{p - p_1}{\frac{1}{2} \rho W^2} = \frac{\frac{p}{p_0} - \frac{p_1}{p_0}}{\frac{\rho W^2}{2 p_0}}$$

and

$$\frac{\rho W^2}{2} = \frac{\gamma p}{2} \frac{\rho W^2}{\gamma p} = \frac{\gamma p}{2} \frac{W^2}{a^2} = \frac{\gamma p}{2} M_1^2$$

where  $M_1$  is the free stream Mach Number.

$$C_p = \frac{\frac{p}{p_0} - \frac{p_1}{p_0}}{\frac{\gamma p}{2 p_0} M_1^2}$$

Across the shock wave, however, there is a drop in stagnation pressure. This drop is defined by  $z = p_3/p_0$  where  $p_3$  corresponds to stagnation conditions behind the shock wave and  $p_0$  corresponds to free stream stagnation conditions.

$$4. \left(\frac{z}{x}\right)^{\frac{\gamma-1}{\gamma}} = 1 + \frac{\gamma-1}{4\gamma \cos^2 \beta} \left[ (\gamma-1) + (\gamma+1) \left(\frac{z}{x}\right) \right]$$

$$\frac{p_1}{p_0} = \frac{1}{\left(1 + \frac{\gamma-1}{2} M_1^2\right)^{\frac{\gamma}{\gamma-1}}}$$

$M_1$ , the free stream Mach Number is known from the Taylor-Maccoll solution of flow around a cone.  $M_s^* = \frac{\text{local velocity}}{\text{critical speed of sound}} = \frac{w}{a^*}$  is known at various points on the surface of the body and

$$(M_s^*)^2 = \frac{\gamma+1}{\gamma-1 + \frac{2}{M_s^2}}$$

or

$$M_s^2 = \frac{2 M_s^{*2}}{(\gamma+1) - (\gamma-1) M_s^{*2}}$$

where  $M_s$  is the Mach number at any point on the surface of the missile. Substituting for  $M_s$  in the equation for  $p_0/p$ :

$$\frac{p_0}{p} = \left[ 1 + \frac{\gamma-1}{2} \left( \frac{2 M_s^{*2}}{(\gamma+1) - (\gamma-1) M_s^{*2}} \right) \right]^{\frac{\gamma}{\gamma-1}}$$

or

$$\frac{p}{p_0} = \left[ 1 - \frac{(\gamma-1)}{(\gamma+1)} M_s^{*2} \right]^{\frac{\gamma}{\gamma-1}}$$

Substituting these quantities into the expression for  $C_p$ :

$$C_p = Z \frac{\frac{p}{p_0} - \frac{p_L}{p_0}}{\frac{\gamma M_1^2}{2} \frac{p_L}{p_0}}$$

$$C_p = Z \left[ \frac{\left(1 - \frac{\gamma-1}{\gamma+1} M_s^{*2}\right)^{\frac{\gamma}{\gamma-1}} - \left(\frac{1}{1 + \frac{\gamma-1}{2} M_1^2}\right)^{\frac{\gamma}{\gamma-1}}}{\frac{\gamma M_1^2}{2} \left(\frac{1}{1 + \frac{\gamma-1}{2} M_1^2}\right)^{\frac{\gamma}{\gamma-1}}}\right]$$

where the only variable for any one free stream  $M_1$  is  $M_9^*$ .

The coefficient of drag,  $C_D$ , is defined for a three dimensional body:

$$C_D = \frac{1}{d^2} \frac{D}{\frac{1}{2} \rho_0 W^2}$$

where  $d$  is the maximum diameter of the body.

$$D = \frac{1}{2} \rho_0 W^2 \int_0^R C_p 2\pi r dr$$

$$C_D = \frac{1}{d^2} \int_0^R 2\pi r C_p dr$$

This integral is numerically evaluated with  $C_p$  being known from the above equation.

## DISCUSSION OF RESULTS

The Sauer Method of Characteristics was applied to the nose section of the Corporal E for free stream Mach numbers of 2 and 4. The shape of the missile was given by the parabola  $r = 15 \left(1 - \frac{x^2}{L^2}\right)$ ,  $L = 96"$ . The result for a free stream Mach number of 3 was obtained from a solution for the same nose section by H. K. Forster. For the case of  $M = 4$  two entirely independent calculations were made to check the consistency of results. In one of these solutions the nose was assumed to be conical for a distance of six inches from the vertex and the constant velocities obtained from the Taylor-Maccoll solution for a cone were assumed to occur over this portion of the nose. In the second of the computations the nose was assumed to be conical for a distance of nine inches from the vertex. It can be seen from the plot of pressure coefficients obtained in Fig. (8) that the results were consistent.

The pressure coefficients obtained for  $M = 2$  and  $M = 4$  are tabulated in Tables IV, V and VI and are plotted in Figs. (8) and (9). For comparison, values of  $C_p$ , obtained by the Karman Moore Method as applied by W. Z. Chien\* to Ogive Nose Sections, are plotted. Figs. (12) and (13). This method makes use of a linearizing process and a close check of results would not be expected. It is noted however that a closer check is obtained at the higher Mach numbers. This is consistent with theory.

Values of the drag coefficients obtained are: At  $M = 2$ ,  $C_D = 0.09168$ , at  $M = 3$ ,  $C_D = .066$ , and at  $M = 4$ ,  $C_D = 0.061$ . These are compared to the values obtained from the Karman Moore Method in Fig. (14).

\*Wave Drag of a Projectile Nose at a Supersonic Velocity by the Karman-Moore Method, ORDCIT Report No. 4-24, April 19, 1946.



All of the points computed in the Mach nets are indicated in Figs. (5), (6), and (7), and the velocities and shock wave angles are tabulated in Tables II and III. (In these tables the velocity is expressed in terms of the critical velocity,  $C^*$ ,  $M^* = \frac{\text{velocity}}{C^*}$ )

The calculation of points and of velocities at these points theoretically could be carried out to any desired degree of accuracy depending on the scale used in the graphical solution. Actually the scale used is limited in the hodograph plane by the size of drafting equipment available. In this instance a twenty-four inch rule calibrated in 1/50 inch increments (5 units equal 1 inch) was used. In the  $M = 4$  solution 50 units correspond to  $M^* = 1$ , and in the  $M = 2$  solution 65 units correspond to  $M^* = 1$ . These scales were chosen so that the full length of the rule would be utilized (and thus maximum accuracy) in the hodograph plane. In the physical plane 5/3 units correspond to 1 inch (i.e. a 1:3 scale).

Following is an outline of the steps in the solution of  $M = 4$  for the Corporal E nose section:

1. Taylor-Maccoll solution\*

- A. A value for  $U/c$  corresponding to  $M = 4$  was chosen from the graph.
- B. A tabular form was set up and indicated calculations were made using increments of  $\phi$  equal to 0.5 degrees.
- C. The angle of the shock wave was solved for in the Taylor-Maccoll region as indicated.
- D. The next step was to solve for the exact free stream Mach number.

\*Taylor, G. I. and Maccoll, J. W., "Air Pressure on a Cone Moving at High Speeds", Proc. of the Roy. Soc., A, Vol. 139, Pages 278-311. 1933.

E. Operations were carried out as indicated in Table VII.

$$M^* = W_{MAX} \sqrt{\frac{\gamma+1}{\gamma-1}} = 2.437 W_{MAX}$$

$M^*$  was converted to the scale in use.

2. The nose section was drawn to the scale chosen.
3. A shock polar was constructed for Mach number 3.9712 as indicated in Fig. (5).
4. Coordinates of the hodograph plane were drawn above the physical plane in such a position as not to interfere with the Mach net.
5. A table of Mach angles and sine squared of the Mach angle was made for anticipated velocities. (See Table VIII).

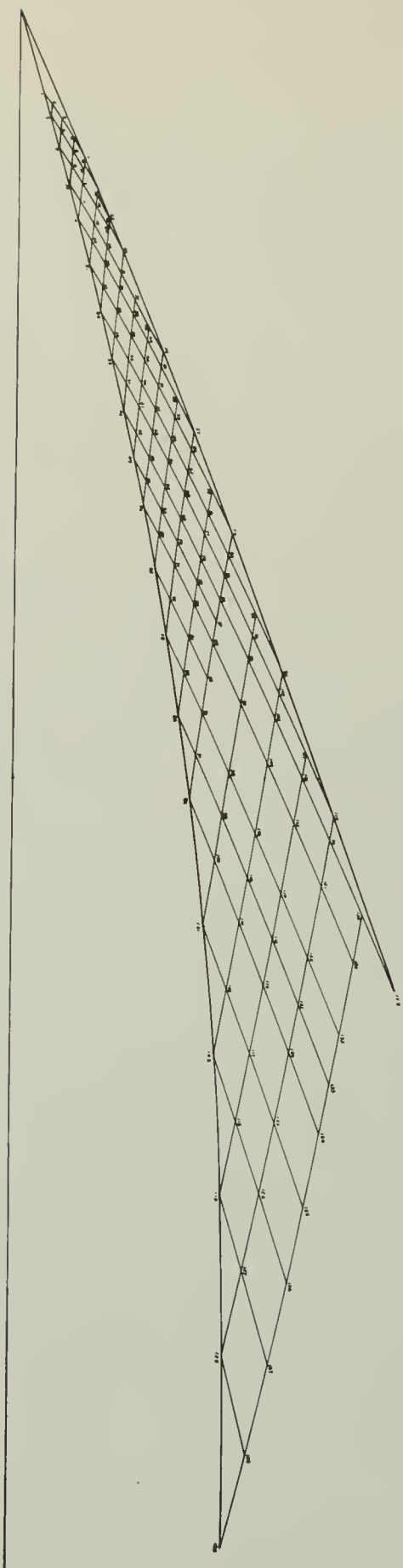
$$\frac{1}{M^2} = \sin^2 \alpha = \frac{1 - \frac{\gamma-1}{\gamma+1} M^{*2}}{\frac{2}{\gamma+1} M^{*2}}$$

6. From Taylor-Maccoll's solution velocities were drafted in the hodograph plane and in the physical plane the  $\eta$  lines were drawn using average values of Mach angle between the points. (Point 1 was taken a distance from the nose corresponding to 6 inches in one case and 9 inches in the other).
7. Calculations of the Mach net by the Sauer Method was started. It was advisable to calculate the slope of the nose at the intersection by a  $\xi$  line from the geometry of the body rather than to approximate it graphically.
8. When a point on the shock wave had to be found the shock polar was placed over the hodograph plane and was removed after the point was located.
9.  $Z$  was calculated. (see Table IX).
10.  $C_p$  was calculated. (see Table IV), and a plot of  $C_p$  vs.  $X$  was made.
11. Even increments of  $X$  were taken and the corresponding values of  $r$  and  $C_p$  were tabulated.

12. A plot  $rC_p$  vs.  $r$ , see Fig. (10), was made and the "positive" area under this curve was determined. This area was connected to the proper scale. (In this case the conversion factor was  $((\frac{3}{5})^2 \times 0.4)$ ).

13. The value for  $C_D = \frac{2\pi}{d^2} \times \text{Area}$  was calculated.

It was found that the most efficient method of constructing the Mach net was to work in pairs. One person drafted while the other performed the calculations. From three to ten points per hour were completed after proficiency in the mechanical processes was obtained. The average working speed was about five points per hour.

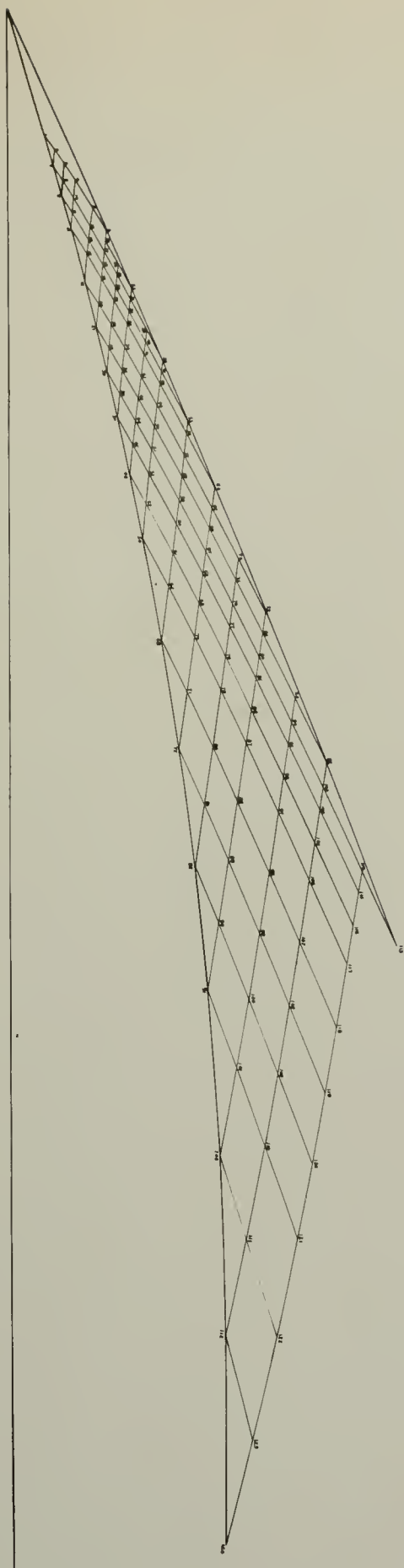


MACH NET FOR  $M = 3.9712$  (Solution I)

Figure (5)

MACH NET FOR  $M = 2.9712$  (Solution II)

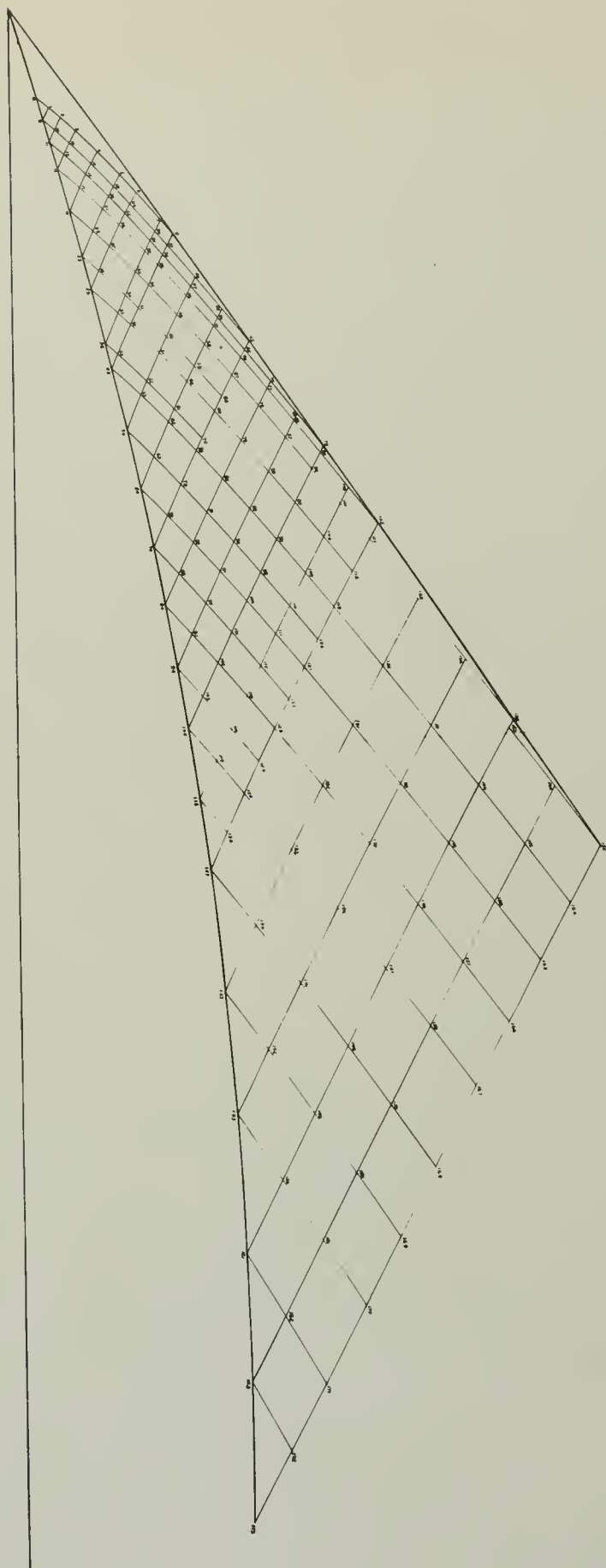
Figure (6)





MACH NET FOR  $M = 2.0039$

Figure (7)





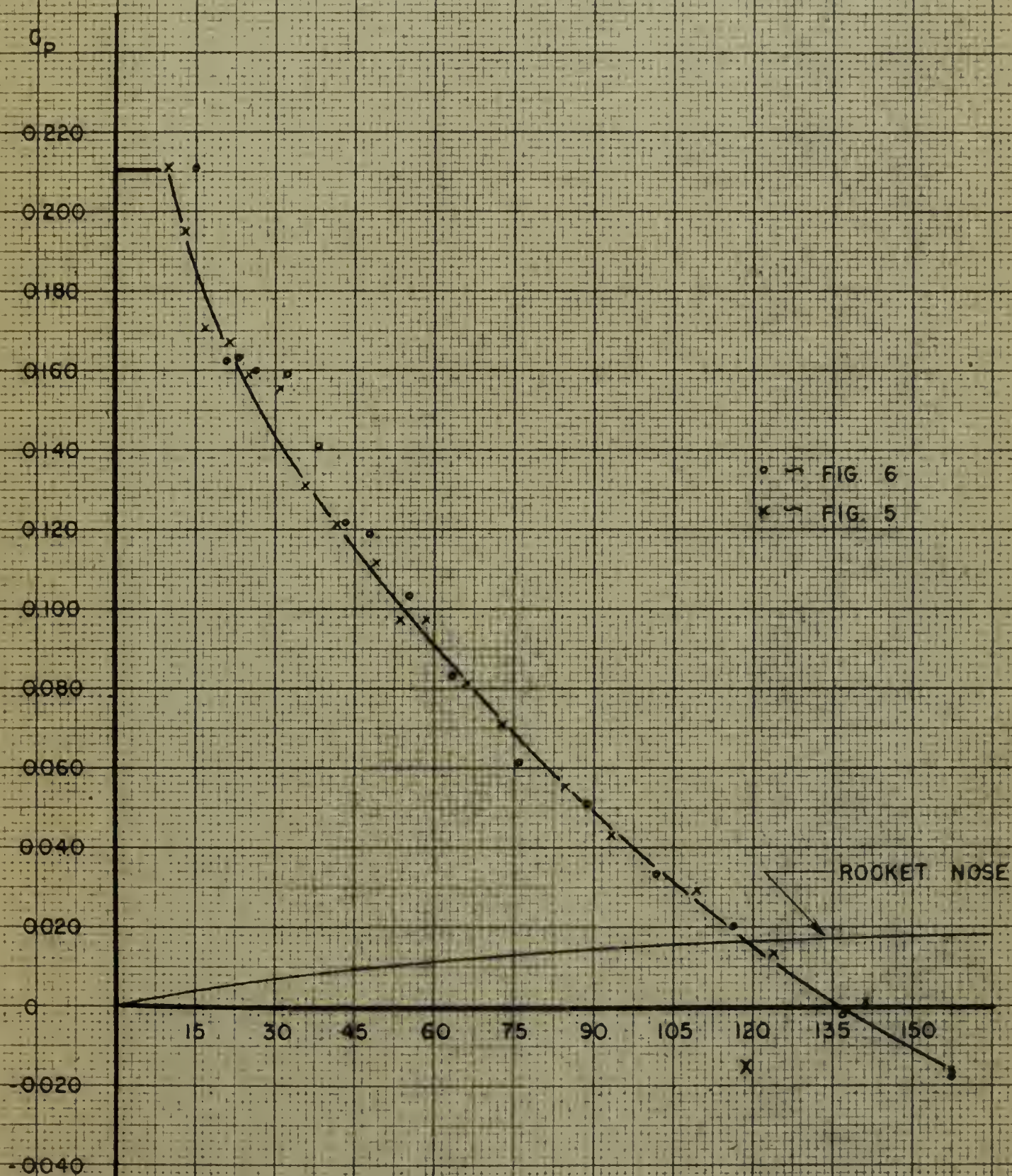
PRESSURE COEFFICIENT FOR  $M = 3.9712$ 

FIGURE 8



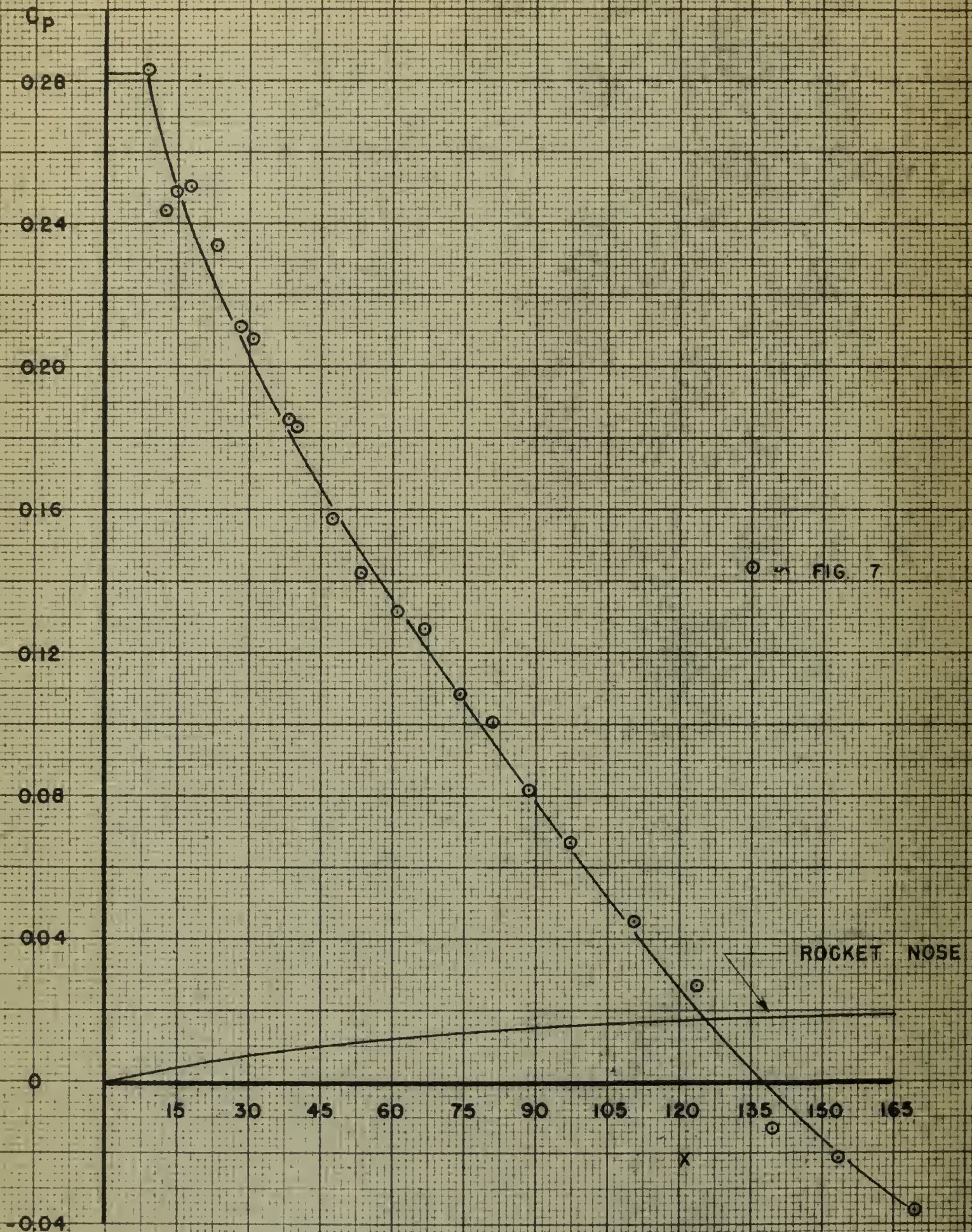
PRESSURE COEFFICIENT FOR  $M = 2.0039$ 

FIGURE 9



$C_p r$  vs  $r$  FOR  $M = 3.9712$

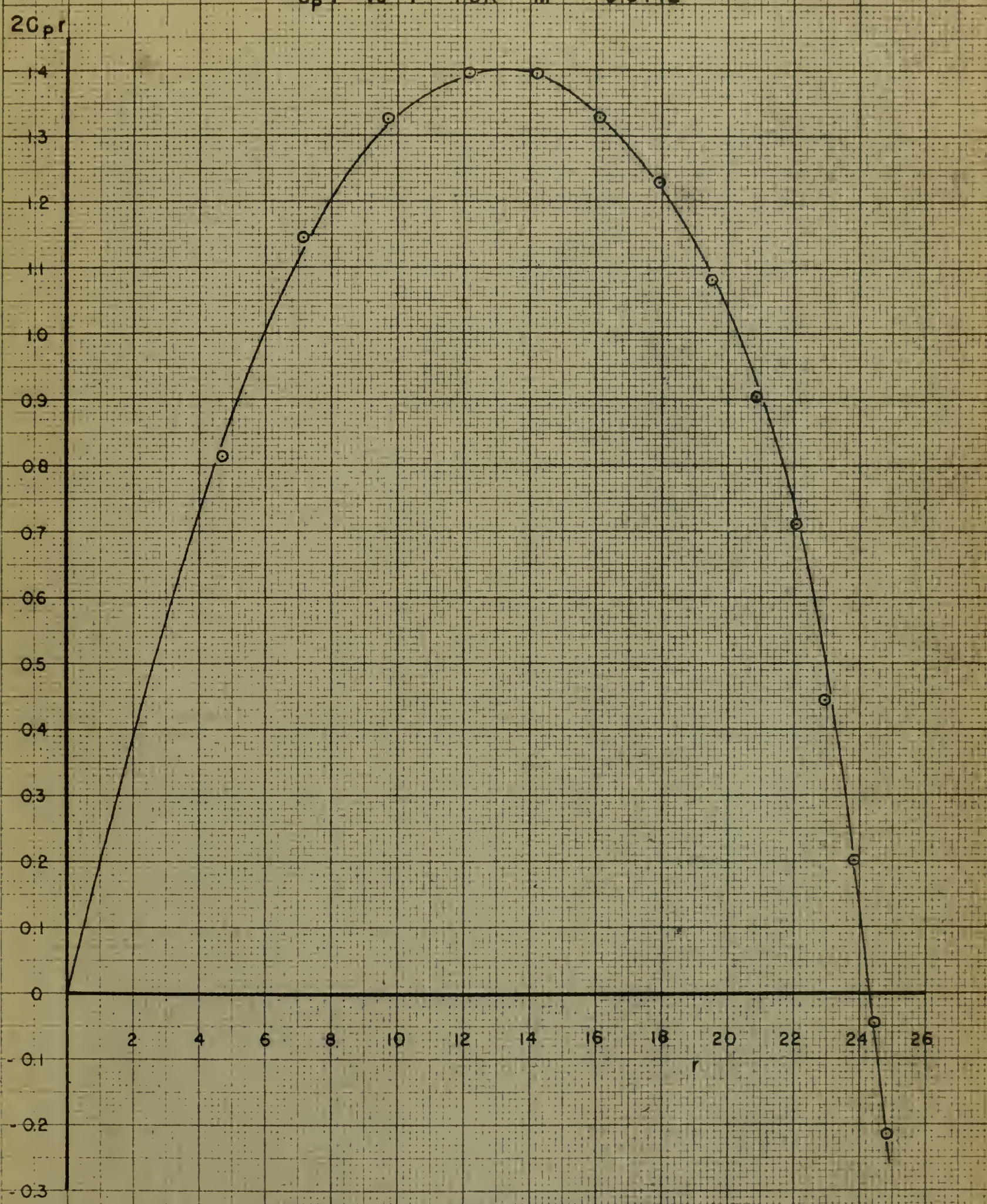


FIGURE 10 (SEE TABLE IV a)



$C_p r$  vs  $r$  FOR  $M = 2.0039$

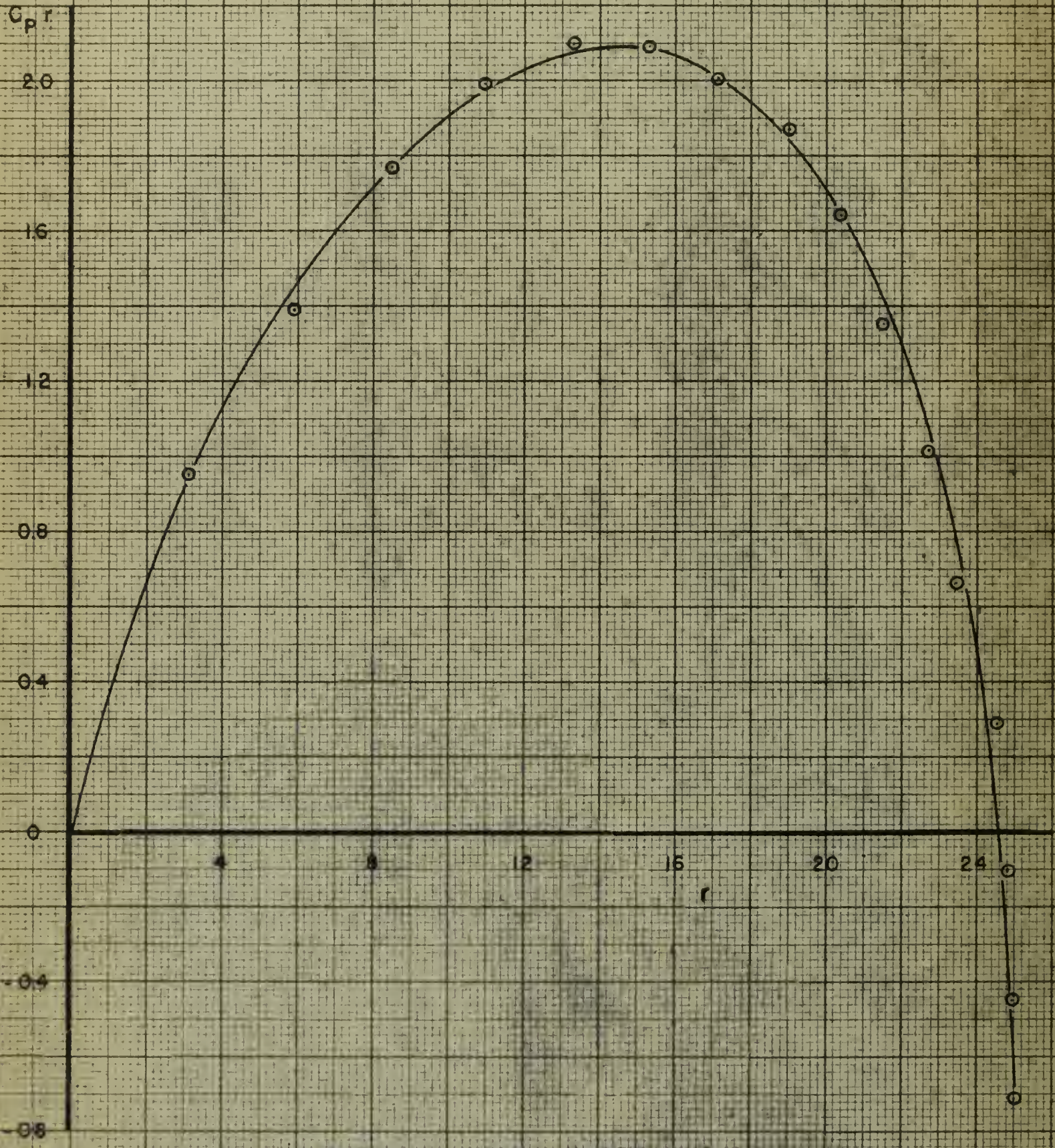


FIGURE 11 (SEE TABLE VI)



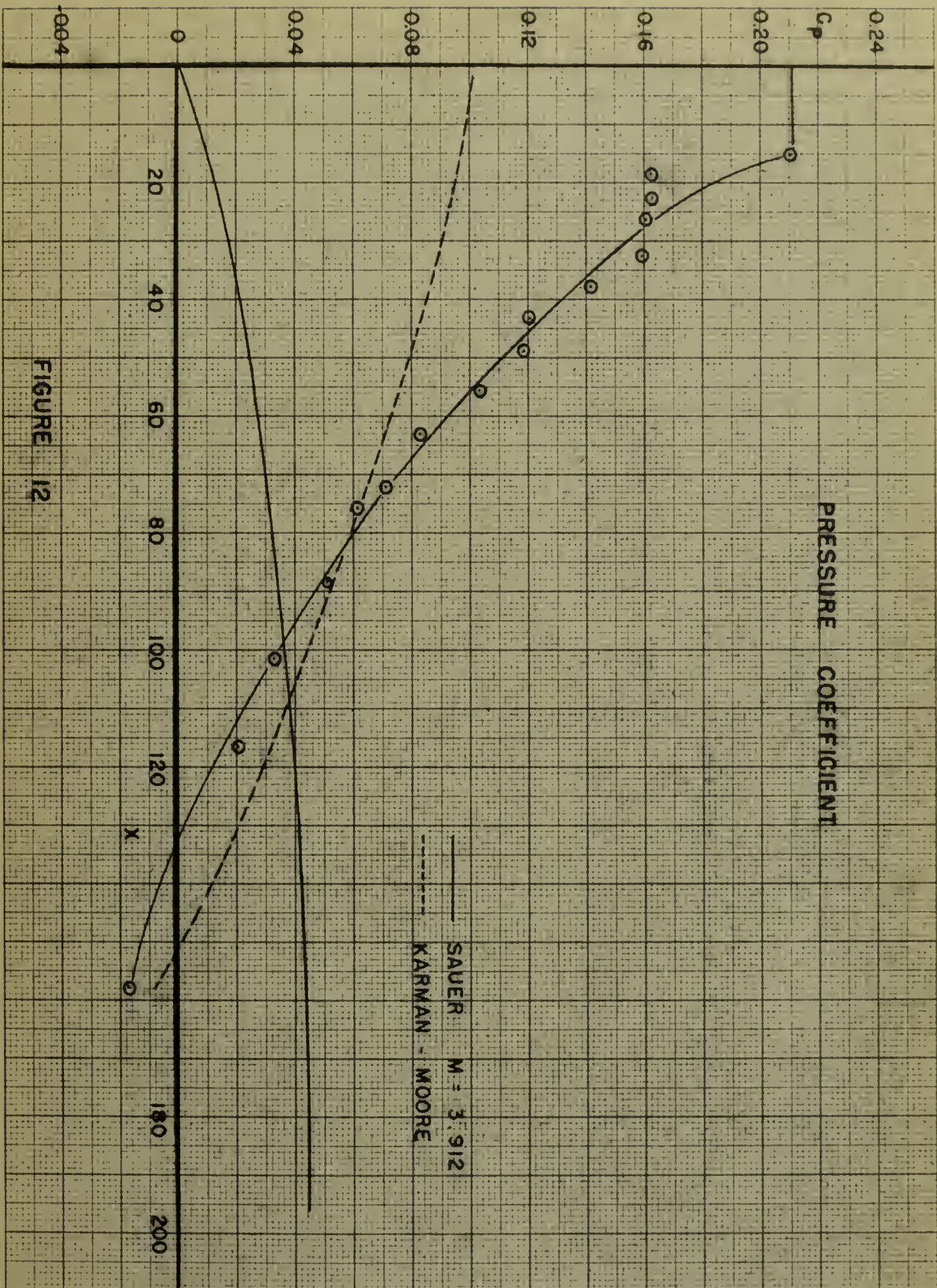


FIGURE 12



# PRESSURE COEFFICIENT

$C_P$  vs  $x$  FOR  $M = 2.0039$

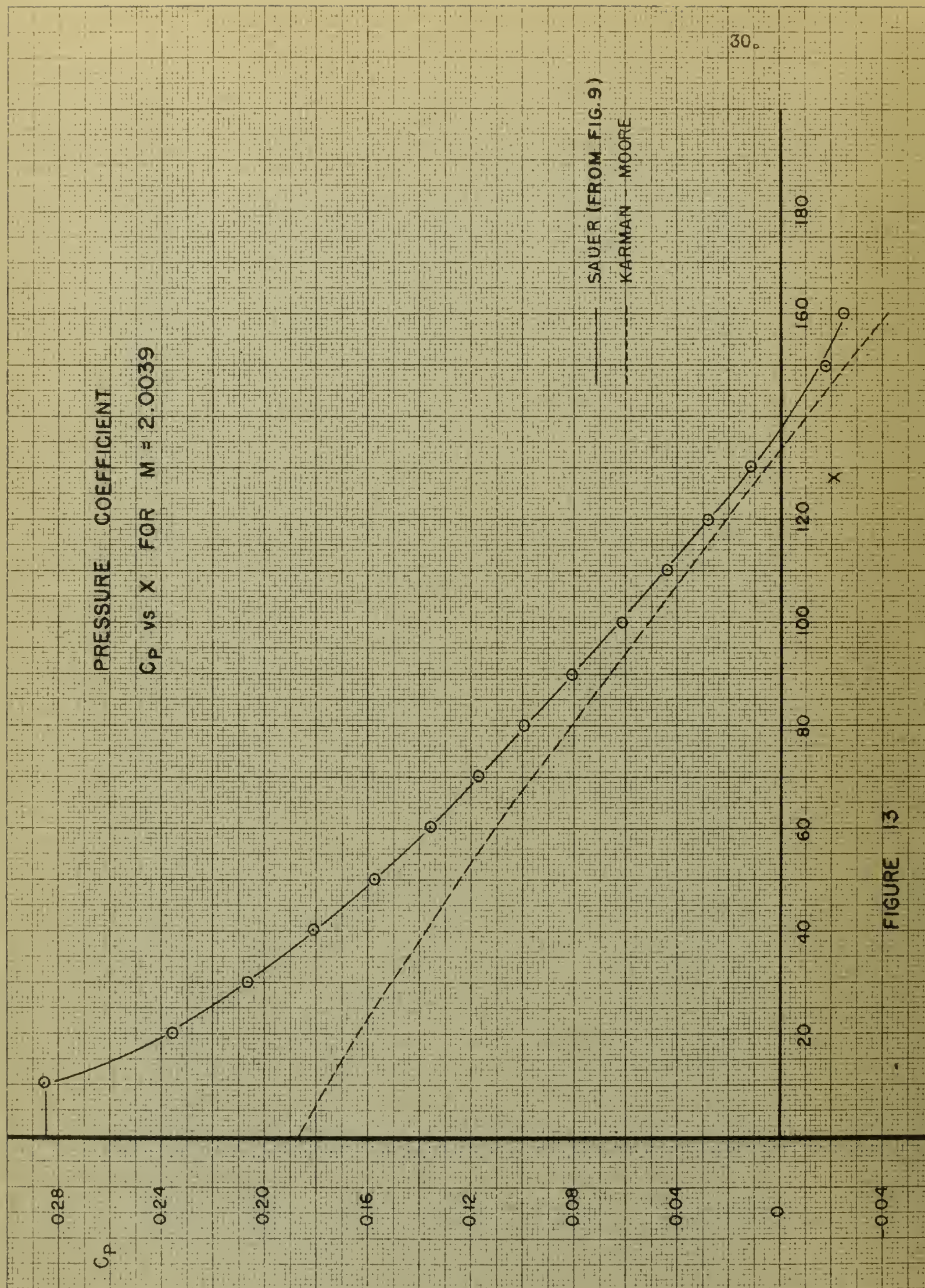
SAUER (FROM FIG. 9)

KARMAN - MOORE

30°

$x$

FIGURE 13





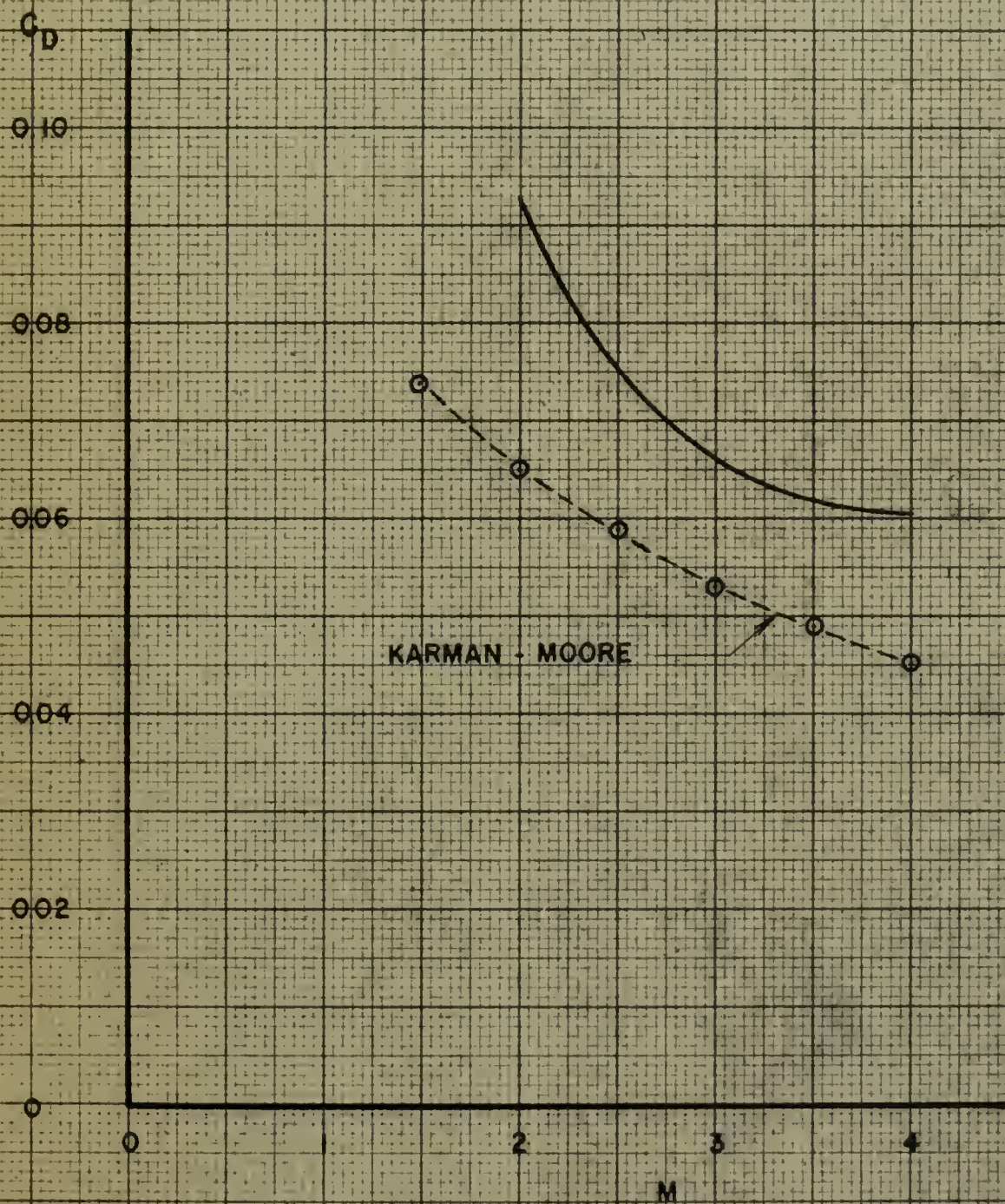
$C_D$  vs  $M$ 

FIGURE 14



In Column 3,  
50 units correspond  
to  $M^* = 1$

TABLE I

SAMPLE TABLE SHOWING DETAILED  
CALCULATIONS FOR MACH NET

| <u>P</u> | <u>P</u>             | <u>M*</u> | <u><math>\delta</math></u> |          | <u><math>\alpha</math></u> |          | <u><math>\sin^2 \alpha</math></u> | <u><math>\sqrt{\phantom{x}}</math></u> |
|----------|----------------------|-----------|----------------------------|----------|----------------------------|----------|-----------------------------------|--|
|          |                      |           | <u>0</u>                   | <u>1</u> | <u>0</u>                   | <u>1</u> |                                   |  |
|          | <sup>1</sup> 69      | 102.05    | 9                          | 15       |                            |          |                                   | 16.35                                  |
|          | <sup>1</sup> 69 - 68 | 101.87    | 9                          | 22       | 17                         | 9        | .0870                             | 16.58                                  |
|          | <sup>1</sup> 69 - 61 | 102.05    | 9                          | 39       | 17                         | 4        | .0862                             | 17.22                                  |
| 69       |                      | 102.05    | 9                          | 15       |                            |          |                                   | 16.35                                  |
|          | <sup>1</sup> 70      | 102.46    | 8                          | 50       |                            |          |                                   | 15.87                                  |
|          | <sup>1</sup> 70 - 69 | 102.25    | 9                          | 2        | 16                         | 57       | .0849                             | 16.11                                  |
|          | <sup>1</sup> 70 - 62 | 102.26    | 9                          | 20       | 16                         | 56       | .0849                             | 16.79                                  |
| 70       |                      | 102.46    | 8                          | 50       |                            |          |                                   | 15.87                                  |
|          | <sup>1</sup> 71      | 103.12    | 8                          | 15       |                            |          |                                   | 14.84                                  |
|          | <sup>1</sup> 71 - 70 | 102.79    | 8                          | 32       | 16                         | 38       | .0819                             | 15.35                                  |
|          | <sup>1</sup> 71 - 63 | 103.22    | 8                          | 50       | 16                         | 24       | .0797                             | 15.96                                  |
| 71       |                      | 103.16    | 8                          | 25       |                            |          |                                   | 15.10                                  |
|          | <sup>1</sup> 72      | 103.88    | 7                          | 58       |                            |          |                                   | 14.46                                  |
|          | <sup>1</sup> 72 - 71 | 103.57    | 8                          | 11       | 16                         | 04       | .0766                             | 14.78                                  |
| 72       |                      | 103.75    | 7                          | 58       |                            |          |                                   | 14.44                                  |
|          | <sup>1</sup> 73      | 101.54    | 8                          | 44       |                            |          |                                   | 15.48                                  |
|          | <sup>1</sup> 73 - 65 | 101.37    | 9                          | 14       | 17                         | 27       | .0899                             | 16.10                                  |
| 73       |                      | 101.54    | 8                          | 44       |                            |          |                                   | 15.48                                  |
| 74       | <sup>1</sup> 65 - 73 | 101.37    | 9                          | 7        |                            |          |                                   | 16.10                                  |
|          | <sup>1</sup> 75      | 101.48    | 8                          | 55       |                            |          |                                   | 15.82                                  |
|          | <sup>1</sup> 75 - 74 | 101.42    | 9                          | 2        | 17                         | 27       | .0899                             | 15.96                                  |
|          | <sup>1</sup> 75 - 66 | 101.40    | 9                          | 27       | 17                         | 27       | .0899                             | 16.32                                  |
| 75       |                      | 101.50    | 9                          | 5        |                            |          |                                   | 16.00                                  |
|          | <sup>1</sup> 76      | 101.72    | 8                          | 52       |                            |          |                                   | 15.80                                  |
|          | <sup>1</sup> 76 - 75 | 101.61    | 8                          | 58       | 17                         | 20       | .0887                             | 15.90                                  |
|          | <sup>1</sup> 76 - 67 | 101.69    | 9                          | 8        | 17                         | 16       | .0881                             | 16.23                                  |
| 76       |                      | 101.72    | 8                          | 52       |                            |          |                                   | 15.80                                  |
|          | <sup>1</sup> 77      | 101.42    | 9                          | 0        |                            |          |                                   | 16.04                                  |
|          | <sup>1</sup> 77 - 76 | 101.57    | 8                          | 56       | 17                         | 21       | .0889                             | 15.92                                  |
|          | <sup>1</sup> 77 - 68 | 101.56    | 9                          | 15       | 17                         | 21       | .0889                             | 16.43                                  |
| 77       |                      | 101.73    | 8                          | 50       |                            |          |                                   | 15.90                                  |
|          | <sup>1</sup> 78      | 102.00    | 8                          | 48       |                            |          |                                   | 15.61                                  |
|          | <sup>1</sup> 78 - 77 | 101.87    | 8                          | 49       | 17                         | 10       | .0872                             | 15.76                                  |
|          | <sup>1</sup> 78 - 69 | 102.03    | 9                          | 02       | 17                         | 05       | .0864                             | 15.98                                  |
| 78       |                      | 102.00    | 8                          | 48       |                            |          |                                   | 15.61                                  |

Point 73 is a point on the shock wave. Point 72 is a point on the missile. All other points are free stream points. P denotes the column for estimated points. The individual estimated points are designated by  $1( )$ ,  $2( )$ , etc.  $1( ) - ( )$  denotes average values between the indicated points.

TABLE I (Cont'd.)

| <u>P</u> | <u>r</u> | <u>dξ</u> | <u>dη</u> | <u>dρ</u> | <u>dσ</u> | <u>Δη</u><br><u>Δ</u> <u>η</u> | <u>Δξ</u><br><u>Δ</u> <u>ξ</u> |
|----------|----------|-----------|-----------|-----------|-----------|--------------------------------|--------------------------------|
|          | 22.40    |           |           |           |           |                                |                                |
|          | 22.65    | 3.52      |           |           | .224      | 26 31                          | -7 47                          |
|          | 20.87    |           |           | .485      |           | 26 43                          | -7 25                          |
| 69       | 22.40    |           |           |           |           |                                |                                |
|          | 21.83    |           |           |           |           |                                |                                |
|          | 22.11    | 3.96      |           |           | .244      | 25 59                          | -7 55                          |
|          | 20.31    |           | 6.90      | .483      |           | 26 16                          | -7 36                          |
| 70       | 21.83    |           |           |           |           |                                |                                |
|          | 20.90    |           |           |           |           |                                |                                |
|          | 21.36    | 6.62      |           |           | .427      | 25 10                          | -8 6                           |
|          | 19.45    |           | 6.82      | .445      |           | 25 14                          | -7 34                          |
| 71       | 20.90    |           |           |           |           |                                |                                |
|          | 19.96    |           |           |           |           |                                |                                |
|          | 20.43    | 6.90      |           |           | .381      | 24 13                          | -7 53                          |
| 72       | 19.96    |           |           |           |           |                                |                                |
|          | 30.34    |           |           |           |           |                                |                                |
|          | 27.18    |           | 14.0      | .745      |           | 26 41                          | 8 13                           |
| 73       | 30.34    |           |           |           |           |                                |                                |
| 74       | 27.18    |           |           |           |           |                                |                                |
|          | 26.82    |           |           |           |           |                                |                                |
|          | 26.95    | 2.38      |           |           | .127      | 26 29                          | -8 25                          |
|          | 25.27    |           | 6.92      | .40       |           | 26 54                          | 8 0                            |
| 75       | 26.82    |           |           |           |           |                                |                                |
|          | 26.40    |           |           |           |           |                                |                                |
|          | 26.61    | 2.83      |           |           | .15       | 26 18                          | -8 22                          |
|          | 24.89    |           | 6.98      | .404      |           | 26 24                          | -8 8                           |
| 76       | 26.40    |           |           |           |           |                                |                                |
|          | 26.00    |           |           |           |           |                                |                                |
|          | 26.20    | 2.65      |           |           | .143      | 26 17                          | -8 25                          |
|          | 24.45    |           | 6.90      | .412      |           | 26 36                          | -8 6                           |
| 77       | 26.00    |           |           |           |           |                                |                                |
|          | 25.50    |           |           |           |           |                                |                                |
|          | 25.75    | 3.75      |           |           | .200      | 25 59                          | -8 21                          |
|          | 23.95    |           | 7.00      | .403      |           | 26 7                           | -8 3                           |
| 78       | 25.50    |           |           |           |           |                                |                                |

TABLE II (a)  
FLOW VELOCITIES FOR

$M = 3.9712$

SIT I

In Column 2

50 units corresponds

to  $M^2 = 1$

| Point | M <sup>2</sup> | $\delta$ |    | Point | M <sup>2</sup> | $\delta$ |    |
|-------|----------------|----------|----|-------|----------------|----------|----|
|       |                | 0        | 1  |       |                | 0        | 1  |
| 1     | 98.60          | 17       | 05 | 46    | 101.79         | 11       | 29 |
| 2     | 98.65          | 15       | 44 | 47    | 101.07         | 9        | 50 |
| 3     | 98.81          | 14       | 28 | 48    | 100.94         | 10       | 10 |
| 4     | 99.05          | 13       | 17 | 49    | 100.94         | 10       | 45 |
| 5     | 99.40          | 12       | 07 | 50    | 101.03         | 10       | 55 |
| 6     | 99.62          | 11       | 30 | 51    | 101.41         | 10       | 50 |
| 7     | 99.93          | 15       | 34 | 52    | 101.51         | 11       | 10 |
| 8     | 99.92          | 13       | 53 | 53    | 102.00         | 10       | 55 |
| 9     | 99.91          | 15       | 02 | 54    | 102.50         | 10       | 49 |
| 10    | 99.95          | 12       | 38 | 55    | 101.30         | 9        | 10 |
| 11    | 99.98          | 13       | 37 | 56    | 101.18         | 9        | 43 |
| 12    | 99.98          | 14       | 37 | 57    | 101.08         | 10       | 07 |
| 13    | 100.17         | 11       | 29 | 58    | 101.27         | 10       | 15 |
| 14    | 100.02         | 12       | 15 | 59    | 101.51         | 10       | 14 |
| 15    | 99.96          | 13       | 00 | 60    | 101.65         | 10       | 15 |
| 16    | 100.08         | 14       | 02 | 61    | 102.05         | 10       | 03 |
| 17    | 100.38         | 10       | 41 | 62    | 102.50         | 9        | 50 |
| 18    | 100.18         | 11       | 25 | 63    | 103.33         | 9        | 25 |
| 19    | 100.10         | 12       | 05 | 64    | 101.30         | 9        | 03 |
| 20    | 100.22         | 13       | 00 | 65    | 101.20         | 9        | 30 |
| 21    | 100.53         | 13       | 25 | 66    | 101.32         | 9        | 32 |
| 22    | 100.00         | 11       | 05 | 67    | 101.57         | 9        | 25 |
| 23    | 100.48         | 10       | 15 | 68    | 101.70         | 9        | 30 |
| 24    | 100.34         | 10       | 40 | 69    | 102.05         | 9        | 15 |
| 25    | 100.60         | 10       | 25 | 70    | 102.46         | 8        | 50 |
| 26    | 100.45         | 10       | 53 | 71    | 103.16         | 8        | 25 |
| 27    | 100.36         | 11       | 30 | 72    | 103.75         | 7        | 58 |
| 28    | 100.45         | 12       | 18 | 73    | 101.54         | 8        | 44 |
| 29    | 100.74         | 12       | 40 | 74    | 101.37         | 9        | 07 |
| 30    | 101.17         | 12       | 50 | 75    | 101.50         | 9        | 05 |
| 31    | 100.82         | 9        | 48 | 76    | 101.72         | 8        | 52 |
| 32    | 100.61         | 10       | 30 | 77    | 101.73         | 8        | 50 |
| 33    | 100.56         | 11       | 0  | 78    | 102.00         | 8        | 48 |
| 34    | 100.55         | 11       | 40 | 79    | 102.48         | 8        | 15 |
| 35    | 100.79         | 11       | 53 | 80    | 103.10         | 7        | 42 |
| 36    | 101.11         | 12       | 01 | 81    | 103.75         | 7        | 24 |
| 37    | 101.25         | 12       | 17 | 82    | 104.60         | 6        | 28 |
| 38    | 101.30         | 9        | 10 | 83    | 101.71         | 8        | 40 |
| 39    | 101.06         | 9        | 29 | 84    | 101.86         | 8        | 33 |
| 40    | 100.79         | 10       | 0  | 85    | 102.00         | 8        | 35 |
| 41    | 100.65         | 10       | 34 | 86    | 102.30         | 8        | 25 |
| 42    | 100.69         | 11       | 04 | 87    | 102.68         | 8        | 0  |
| 43    | 100.88         | 11       | 13 | 88    | 103.24         | 7        | 25 |
| 44    | 101.17         | 11       | 17 | 89    | 103.78         | 6        | 53 |
| 45    | 101.37         | 11       | 35 | 90    | 104.61         | 5        | 53 |

TABLE II (a) Cont'd.

| Point | M <sup>o</sup> | $\int$ |    |
|-------|----------------|--------|----|
|       |                | 2      | 1  |
| 91    | 105.24         | 4      | 50 |
| 92    | 101.96         | 8      | 0  |
| 93    | 101.83         | 8      | 20 |
| 94    | 102.00         | 8      | 10 |
| 95    | 102.15         | 8      | 15 |
| 96    | 102.31         | 8      | 0  |
| 97    | 102.70         | 7      | 40 |
| 98    | 103.35         | 7      | 05 |
| 99    | 103.85         | 6      | 25 |
| 100   | 104.65         | 5      | 30 |
| 101   | 105.30         | 4      | 38 |
| 102   | 106.44         | 2      | 40 |
| 103   | 102.13         | 7      | 48 |
| 104   | 102.15         | 7      | 45 |
| 105   | 102.43         | 7      | 48 |
| 106   | 102.78         | 7      | 19 |
| 107   | 103.41         | 6      | 35 |
| 108   | 103.98         | 6      | 01 |
| 109   | 104.75         | 5      | 03 |
| 110   | 105.28         | 4      | 05 |
| 111   | 106.33         | 2      | 21 |
| 112   | 107.49         | 0      | 18 |
| 113   | 102.45         | 7      | 20 |
| 114   | 102.29         | 7      | 34 |
| 115   | 102.44         | 7      | 25 |
| 116   | 102.56         | 7      | 15 |
| 117   | 102.93         | 6      | 53 |
| 118   | 103.43         | 6      | 10 |
| 119   | 103.98         | 5      | 30 |
| 120   | 104.64         | 4      | 30 |
| 121   | 105.25         | 3      | 35 |
| 122   | 106.28         | 1      | 50 |
| 123   | 107.25         | 0      | 12 |
| 124   | 107.18         | 0      | 0  |



In Column 2,  
50 units corresponds  
to  $M^* = 1$

TABLE II (b)  
FLOW VELOCITIES FOR  $M = 3.9712$   
SET II

| Point | $M^*$  | $\int$ |    | Point | $M^*$  | $\int$ |    |
|-------|--------|--------|----|-------|--------|--------|----|
|       |        | 0      | 1  |       |        | 0      | 1  |
| 1     | 98.60  | 17     | 08 | 46    | 101.10 | 11     | 10 |
| 2     | 98.75  | 15     | 18 | 47    | 101.45 | 11     | 20 |
| 3     | 98.97  | 13     | 41 | 48    | 101.60 | 11     | 45 |
| 4     | 99.40  | 12     | 07 | 49    | 102.00 | 11     | 50 |
| 5     | 99.50  | 16     | 05 | 50    | 101.00 | 9      | 45 |
| 6     | 99.55  | 13     | 55 | 51    | 101.00 | 10     | 25 |
| 7     | 99.70  | 15     | 42 | 52    | 101.10 | 10     | 30 |
| 8     | 99.90  | 12     | 10 | 53    | 101.40 | 10     | 34 |
| 9     | 99.40  | 14     | 00 | 54    | 101.55 | 10     | 45 |
| 10    | 99.80  | 15     | 13 | 55    | 101.85 | 10     | 45 |
| 11    | 99.62  | 11     | 30 | 56    | 102.00 | 11     | 13 |
| 12    | 100.10 | 11     | 25 | 57    | 101.25 | 8      | 50 |
| 13    | 99.55  | 13     | 00 | 58    | 101.12 | 9      | 18 |
| 14    | 99.85  | 13     | 50 | 59    | 101.10 | 9      | 45 |
| 15    | 100.00 | 14     | 47 | 60    | 101.25 | 9      | 50 |
| 16    | 99.86  | 11     | 28 | 61    | 101.50 | 10     | 00 |
| 17    | 100.15 | 10     | 30 | 62    | 101.60 | 10     | 15 |
| 18    | 99.85  | 11     | 45 | 63    | 101.90 | 10     | 20 |
| 19    | 100.00 | 12     | 15 | 64    | 102.00 | 10     | 40 |
| 20    | 100.00 | 13     | 15 | 65    | 102.60 | 10     | 24 |
| 21    | 100.15 | 14     | 12 | 66    | 101.30 | 9      | 15 |
| 22    | 100.05 | 10     | 55 | 67    | 101.40 | 9      | 30 |
| 23    | 100.35 | 10     | 15 | 68    | 101.65 | 9      | 30 |
| 24    | 100.10 | 11     | 25 | 69    | 101.70 | 9      | 45 |
| 25    | 100.20 | 11     | 45 | 70    | 102.10 | 9      | 55 |
| 26    | 100.25 | 12     | 25 | 71    | 102.20 | 10     | 10 |
| 27    | 100.35 | 13     | 20 | 72    | 102.60 | 9      | 55 |
| 28    | 100.90 | 13     | 40 | 73    | 103.00 | 9      | 53 |
| 29    | 100.19 | 11     | 02 | 74    | 101.60 | 8      | 15 |
| 30    | 100.35 | 10     | 15 | 75    | 101.45 | 8      | 45 |
| 31    | 100.35 | 10     | 50 | 76    | 101.60 | 8      | 55 |
| 32    | 100.40 | 11     | 40 | 77    | 101.70 | 8      | 51 |
| 33    | 100.50 | 12     | 15 | 78    | 101.90 | 9      | 07 |
| 34    | 100.90 | 12     | 32 | 79    | 102.20 | 8      | 55 |
| 35    | 101.20 | 13     | 02 | 80    | 102.30 | 9      | 15 |
| 36    | 100.90 | 9      | 30 | 81    | 102.65 | 9      | 00 |
| 37    | 100.53 | 10     | 23 | 82    | 103.00 | 9      | 05 |
| 38    | 100.60 | 10     | 45 | 83    | 103.60 | 8      | 30 |
| 39    | 100.60 | 11     | 35 | 84    | 101.80 | 8      | 25 |
| 40    | 101.00 | 11     | 45 | 85    | 101.95 | 8      | 20 |
| 41    | 101.40 | 12     | 0  | 86    | 102.00 | 8      | 50 |
| 42    | 101.50 | 12     | 25 | 87    | 102.25 | 8      | 45 |
| 43    | 101.72 | 9      | 56 | 88    | 102.40 | 8      | 50 |
| 44    | 100.90 | 10     | 12 | 89    | 102.70 | 8      | 40 |
| 45    | 100.90 | 10     | 55 | 90    | 103.05 | 8      | 30 |

TABLE II (b) Cont'd.

| Point | M <sup>W</sup> | $\int$ | '  |
|-------|----------------|--------|----|
| 91    | 103.60         | 8      | 10 |
| 92    | 104.15         | 7      | 33 |
| 93    | 102.10         | 7      | 35 |
| 94    | 101.95         | 8      | 00 |
| 95    | 102.00         | 8      | 10 |
| 96    | 102.05         | 8      | 15 |
| 97    | 102.30         | 8      | 05 |
| 98    | 102.95         | 7      | 32 |
| 99    | 103.95         | 7      | 00 |
| 100   | 104.00         | 6      | 45 |
| 101   | 104.80         | 5      | 50 |
| 102   | 102.10         | 7      | 50 |
| 103   | 102.20         | 7      | 50 |
| 104   | 102.50         | 7      | 42 |
| 105   | 103.00         | 7      | 00 |
| 106   | 103.55         | 6      | 15 |
| 107   | 104.05         | 6      | 10 |
| 108   | 104.85         | 5      | 15 |
| 109   | 105.55         | 4      | 10 |
| 110   | 102.30         | 7      | 00 |
| 111   | 102.20         | 7      | 25 |
| 112   | 102.40         | 7      | 30 |
| 113   | 102.60         | 7      | 13 |
| 114   | 103.10         | 6      | 40 |
| 115   | 103.65         | 6      | 12 |
| 116   | 104.10         | 5      | 45 |
| 117   | 104.80         | 4      | 45 |
| 118   | 105.50         | 3      | 50 |
| 119   | 106.30         | 2      | 20 |
| 120   | 102.35         | 7      | 10 |
| 121   | 102.65         | 7      | 00 |
| 122   | 103.20         | 6      | 25 |
| 123   | 103.70         | 5      | 55 |
| 124   | 104.10         | 5      | 25 |
| 125   | 104.95         | 4      | 30 |
| 126   | 105.45         | 3      | 38 |
| 127   | 106.30         | 2      | 16 |
| 128   | 107.30         | 0      | 12 |
| 129   | 102.60         | 6      | 50 |
| 130   | 102.48         | 7      | 00 |
| 131   | 102.85         | 6      | 45 |
| 132   | 103.30         | 6      | 20 |
| 133   | 103.80         | 5      | 40 |
| 134   | 104.35         | 5      | 10 |
| 135   | 105.00         | 4      | 05 |
| 136   | 105.65         | 3      | 20 |
| 137   | 106.40         | 2      | 00 |
| 138   | 107.40         | 0      | 05 |
| 139   | 107.50         | 0      | 0  |

In Column 2,  
65 units corresponds  
to  $M^* = 1$

38.

TABLE III  
FLOW VELOCITIES FOR  $M = 2.0039$

| Point | $M^*$ | $\delta$ |    | Point | $M^*$  | $\delta$ |    |
|-------|-------|----------|----|-------|--------|----------|----|
|       |       | 2        | 1  |       |        | 2        | 1  |
| 1     | 94.90 | 13       | 46 | 46    | 99.38  | 6        | 13 |
| 2     | 95.65 | 11       | 19 | 47    | 99.60  | 6        | 20 |
| 3     | 96.38 | 9        | 47 | 48    | 99.05  | 7        | 00 |
| 4     | 97.28 | 8        | 22 | 49    | 99.70  | 7        | 55 |
| 5     | 98.01 | 7        | 25 | 50    | 98.70  | 8        | 30 |
| 6     | 99.44 | 6        | 55 | 51    | 98.65  | 9        | 10 |
| 7     | 98.94 | 6        | 22 | 52    | 98.90  | 10       | 20 |
| 8     | 99.19 | 6        | 05 | 53    | 99.00  | 11       | 00 |
| 9     | 96.05 | 16       | 03 | 54    | 99.69  | 12       | 25 |
| 10    | 96.20 | 12       | 40 | 55    | 99.58  | 5        | 56 |
| 11    | 95.90 | 15       | 49 | 56    | 99.95  | 6        | 50 |
| 12    | 96.65 | 10       | 35 | 57    | 99.40  | 6        | 35 |
| 13    | 96.20 | 12       | 35 | 58    | 99.10  | 7        | 20 |
| 14    | 95.85 | 15       | 30 | 59    | 99.20  | 7        | 45 |
| 15    | 97.40 | 8        | 55 | 60    | 99.10  | 8        | 15 |
| 16    | 97.00 | 10       | 10 | 61    | 99.10  | 9        | 5  |
| 17    | 96.30 | 11       | 58 | 62    | 99.15  | 9        | 30 |
| 18    | 96.50 | 15       | 00 | 63    | 99.70  | 10       | 30 |
| 19    | 97.30 | 8        | 00 | 64    | 100.35 | 11       | 43 |
| 20    | 97.65 | 8        | 45 | 65    | 100.25 | 5        | 30 |
| 21    | 97.05 | 10       | 05 | 66    | 99.80  | 6        | 10 |
| 22    | 96.85 | 12       | 01 | 67    | 99.50  | 6        | 50 |
| 23    | 97.30 | 14       | 28 | 68    | 99.55  | 7        | 14 |
| 24    | 98.35 | 7        | 25 | 69    | 99.45  | 7        | 37 |
| 25    | 98.10 | 8        | 00 | 70    | 99.45  | 8        | 12 |
| 26    | 97.50 | 9        | 05 | 71    | 99.50  | 8        | 40 |
| 27    | 97.20 | 10       | 35 | 72    | 99.90  | 9        | 20 |
| 28    | 97.40 | 12       | 20 | 73    | 100.20 | 10       | 00 |
| 29    | 97.55 | 14       | 05 | 74    | 100.80 | 11       | 00 |
| 30    | 98.75 | 6        | 50 | 75    | 100.80 | 4        | 35 |
| 31    | 98.65 | 7        | 12 | 76    | 100.43 | 5        | 12 |
| 32    | 98.15 | 8        | 00 | 77    | 100.10 | 5        | 40 |
| 33    | 97.80 | 9        | 15 | 78    | 99.80  | 6        | 10 |
| 34    | 97.95 | 10       | 20 | 79    | 99.50  | 7        | 00 |
| 35    | 98.00 | 11       | 30 | 80    | 99.40  | 7        | 40 |
| 36    | 98.50 | 13       | 28 | 81    | 99.85  | 8        | 15 |
| 37    | 99.10 | 6        | 30 | 82    | 100.15 | 8        | 50 |
| 38    | 99.00 | 6        | 50 | 83    | 101.00 | 9        | 00 |
| 39    | 98.50 | 7        | 40 | 84    | 101.00 | 10       | 18 |
| 40    | 97.95 | 8        | 40 | 85    | 100.62 | 4        | 54 |
| 41    | 98.15 | 9        | 40 | 86    | 100.30 | 5        | 25 |
| 42    | 98.20 | 10       | 25 | 87    | 100.10 | 5        | 40 |
| 43    | 98.50 | 12       | 00 | 88    | 99.80  | 6        | 30 |
| 44    | 98.60 | 13       | 10 | 89    | 99.75  | 7        | 10 |
| 45    | 99.78 | 5        | 40 | 90    | 100.05 | 7        | 30 |



TABLE III (Cont'd.)

| Point | M <sup>a</sup> | $\delta$ |    | Point | M <sup>a</sup> | $\delta$ |    |
|-------|----------------|----------|----|-------|----------------|----------|----|
|       |                | 2        | 1  |       |                | 2        | 1  |
| 91    | 100.30         | 7        | 50 | 140   | 102.00         | 5        | 10 |
| 92    | 100.95         | 8        | 00 | 141   | 103.45         | 4        | 45 |
| 93    | 100.30         | 8        | 55 | 142   | 104.45         | 4        | 30 |
| 94    | 101.80         | 9        | 33 | 143   | 105.65         | 4        | 06 |
| 95    | 100.50         | 5        | 05 | 144   | 101.20         | 4        | 30 |
| 96    | 100.30         | 5        | 25 | 145   | 101.35         | 4        | 50 |
| 97    | 100.20         | 5        | 45 | 146   | 101.80         | 4        | 55 |
| 98    | 99.85          | 6        | 30 | 147   | 102.35         | 5        | 00 |
| 99    | 100.10         | 6        | 50 | 148   | 103.75         | 4        | 30 |
| 100   | 100.30         | 7        | 15 | 149   | 104.80         | 4        | 05 |
| 101   | 101.20         | 7        | 10 | 150   | 105.90         | 3        | 40 |
| 102   | 100.95         | 8        | 00 | 151   | 107.80         | 3        | 21 |
| 103   | 101.55         | 8        | 20 | 152   | 101.24         | 4        | 08 |
| 104   | 102.20         | 8        | 48 | 153   | 101.65         | 3        | 45 |
| 105   | 100.75         | 4        | 30 | 154   | 101.44         | 3        | 56 |
| 106   | 100.62         | 4        | 48 | 155   | 101.35         | 4        | 10 |
| 107   | 100.50         | 5        | 05 | 156   | 101.40         | 4        | 25 |
| 108   | 100.35         | 5        | 25 | 157   | 101.80         | 4        | 20 |
| 109   | 100.30         | 6        | 00 | 158   | 102.35         | 4        | 20 |
| 110   | 100.40         | 6        | 20 | 159   | 103.70         | 3        | 45 |
| 111   | 100.55         | 6        | 40 | 160   | 104.65         | 3        | 20 |
| 112   | 101.35         | 6        | 35 | 161   | 105.70         | 2        | 50 |
| 113   | 101.20         | 7        | 10 | 162   | 107.45         | 1        | 35 |
| 114   | 101.65         | 7        | 30 | 163   | 108.20         | 0        | 46 |
| 115   | 102.20         | 7        | 45 | 164   | 101.65         | 4        | 00 |
| 116   | 103.05         | 7        | 57 | 165   | 101.75         | 4        | 15 |
| 117   | 100.62         | 4        | 48 | 166   | 102.10         | 4        | 10 |
| 118   | 100.45         | 5        | 05 | 167   | 102.60         | 4        | 05 |
| 119   | 100.45         | 5        | 30 | 168   | 103.80         | 4        | 30 |
| 120   | 100.50         | 6        | 00 | 169   | 104.70         | 3        | 00 |
| 121   | 100.60         | 6        | 15 | 170   | 105.70         | 2        | 30 |
| 122   | 101.40         | 6        | 00 | 171   | 107.40         | 1        | 12 |
| 123   | 101.35         | 6        | 35 | 172   | 108.25         | 0        | 45 |
| 124   | 101.65         | 6        | 50 | 173   | 109.00         | 0        | 00 |
| 125   | 102.00         | 7        | 05 |       |                |          |    |
| 126   | 102.80         | 7        | 05 |       |                |          |    |
| 127   | 103.75         | 7        | 05 |       |                |          |    |
| 128   | 101.25         | 4        | 05 |       |                |          |    |
| 129   | 100.83         | 4        | 34 |       |                |          |    |
| 130   | 100.75         | 5        | 10 |       |                |          |    |
| 131   | 100.80         | 5        | 35 |       |                |          |    |
| 132   | 101.40         | 5        | 50 |       |                |          |    |
| 133   | 102.05         | 6        | 05 |       |                |          |    |
| 134   | 103.60         | 5        | 50 |       |                |          |    |
| 135   | 104.80         | 5        | 37 |       |                |          |    |
| 136   | 100.04         | 4        | 20 |       |                |          |    |
| 137   | 100.70         | 4        | 35 |       |                |          |    |
| 138   | 100.80         | 5        | 00 |       |                |          |    |
| 139   | 101.35         | 5        | 10 |       |                |          |    |

TABLE IV  
DATA SHEET  
FOR CALCULATION  
OF  $C_p$  FOR  $M = 3.9712$   
(CORRESPONDING TO FIG. (6)).

| Point | Coordinates |       | 50 $M^*$ | $M^*$  | $C_p$  | $2\pi C_p$ |
|-------|-------------|-------|----------|--------|--------|------------|
|       | $x$         | $z$   |          |        |        |            |
| 1     | 15          | 4.36  | 98.60    | 1.9720 | .2109  | 1.83905    |
| 7     | 18.83       | 5.48  | 99.93    | 1.9986 | .1621  | 1.97662    |
| 9     | 22.32       | 6.45  | 99.91    | 1.9982 | .1634  | 2.10786    |
| 12    | 26.23       | 7.49  | 99.98    | 1.9996 | .1604  | 2.40279    |
| 16    | 32.62       | 9.15  | 100.08   | 2.0016 | .1596  | 2.92058    |
| 21    | 37.96       | 10.45 | 100.53   | 2.0106 | .1419  | 2.96571    |
| 30    | 43.19       | 11.67 | 101.17   | 2.0234 | .1218  | 2.84281    |
| 37    | 48.74       | 12.96 | 101.25   | 2.0250 | .1192  | 3.08966    |
| 46    | 55.48       | 14.34 | 101.79   | 2.0358 | .1032  | 2.95978    |
| 54    | 63.05       | 15.78 | 102.50   | 2.0500 | .0833  | 2.62895    |
| 63    | 75.20       | 18.00 | 103.33   | 2.0666 | .0619  | 2.22840    |
| 72    | 88.17       | 19.96 | 103.75   | 2.0750 | .0519  | 2.07185    |
| 82    | 101.97      | 21.75 | 104.60   | 2.0920 | .0330  | 1.43550    |
| 91    | 116.63      | 23.12 | 105.24   | 2.1048 | .0201  | 0.92942    |
| 102   | 136.40      | 24.46 | 106.44   | 2.1288 | -.0016 | -0.78272   |
| 112   | 157.52      | 24.98 | 107.49   | 2.1498 | -.0178 | -0.88929   |
| 124   | 182.10      | 25.00 | 107.18   | 2.1436 | -.0133 | -0.66500   |

TABLE V  
DATA SHEET FOR CALCULATION OF  $C_p$  FOR  $M = 3.9712$   
CORRESPONDING TO FIG. (5)

| Point | x      | R     | 50 $M^*$ | $M^*$ | $C_p$  | $r_{C_p}^*$ |
|-------|--------|-------|----------|-------|--------|-------------|
| 1     | 10     | 3.03  | 98.6     | 1.972 | .2109  | .6390       |
| 5     | 12.60  | 3.80  | 99.5     | 1.980 | .1957  | .7436       |
| 7     | 16.20  | 4.75  | 99.70    | 1.994 | .1701  | .8079       |
| 10    | 20.60  | 6.00  | 99.80    | 1.996 | .1666  | .9996       |
| 15    | 24.85  | 7.10  | 100.00   | 2.000 | .1597  | 1.1333      |
| 21    | 30.20  | 8.45  | 100.15   | 2.003 | .1546  | 1.3063      |
| 28    | 35.60  | 9.75  | 100.90   | 2.018 | .1301  | 1.2684      |
| 35    | 41.15  | 11.10 | 101.20   | 2.020 | .1207  | 1.3397      |
| 42    | 47.20  | 12.60 | 101.50   | 2.030 | .1116  | 1.3950      |
| 49    | 52.80  | 13.80 | 102.00   | 2.040 | .0971  | 1.3400      |
| 56    | 58.30  | 14.95 | 102.00   | 2.040 | .0971  | 1.4516      |
| 65    | 65.90  | 16.40 | 102.60   | 2.052 | .0806  | 1.3218      |
| 73    | 73.70  | 17.70 | 103.00   | 2.060 | .0702  | 1.2425      |
| 83    | 83.30  | 19.30 | 103.60   | 2.072 | .0554  | 1.0692      |
| 92    | 93.00  | 20.65 | 104.15   | 2.083 | .0428  | .8338       |
| 101   | 107.80 | 22.30 | 104.80   | 2.096 | .0287  | .6400       |
| 109   | 122.80 | 23.70 | 105.55   | 2.112 | .0132  | .3128       |
| 119   | 139.10 | 24.60 | 106.30   | 2.126 | .0007  | .0172       |
| 128   | 157.65 | 24.85 | 107.30   | 2.146 | -.0151 | -0.3752     |
| 139   | 180.80 | 25.00 | 107.50   | 2.150 | -.0179 | -0.4475     |



TABLE VI  
DATA SHEET FOR CALCULATION OF  $C_p$  FOR  $M = 2.0039$

CORRESPONDING TO FIG. (9)

| Point | x      | r     | 65 M*  | M*       | $C_p$   | $rC_p$ |
|-------|--------|-------|--------|----------|---------|--------|
| 0     | 10.00  | 3.08  | 94.57  | 1.454922 | .28291  | 0.871  |
| 9     | 12.40  | 3.80  | 96.05  | 1.477692 | .24400  | 0.927  |
| 11    | 16.00  | 4.50  | 95.90  | 1.475384 | .24292  | 1.121  |
| 14    | 18.00  | 5.35  | 95.85  | 1.474615 | .25051  | 1.340  |
| 18    | 22.80  | 6.65  | 96.50  | 1.484615 | .23419  | 1.557  |
| 23    | 27.90  | 7.95  | 97.30  | 1.496923 | .21442  | 1.705  |
| 29    | 31.50  | 8.85  | 97.55  | 1.500769 | .20831  | 1.844  |
| 36    | 37.60  | 10.30 | 98.50  | 1.515538 | .18513  | 1.907  |
| 44    | 40.50  | 11.00 | 98.60  | 1.516923 | .18299  | 2.013  |
| 54    | 47.30  | 12.60 | 99.65  | 1.533076 | .15822  | 1.994  |
| 64    | 53.80  | 14.00 | 100.35 | 1.543846 | .14205  | 1.989  |
| 74    | 60.50  | 15.40 | 100.80 | 1.550769 | .13178  | 2.029  |
| 84    | 67.00  | 16.55 | 101.00 | 1.553846 | .12724  | 2.106  |
| 94    | 74.00  | 17.80 | 101.80 | 1.566153 | .10934  | 1.946  |
| 104   | 80.80  | 18.90 | 102.20 | 1.572307 | .10053  | 1.900  |
| 116   | 88.70  | 20.10 | 103.05 | 1.585384 | .08205  | 1.649  |
| 127   | 96.40  | 21.10 | 103.75 | 1.596153 | .06732  | 1.420  |
| 135   | 110.00 | 22.60 | 104.80 | 1.612307 | .04528  | 1.023  |
| 143   | 123.60 | 23.90 | 105.65 | 1.625384 | .02805  | 0.670  |
| 151   | 139.10 | 24.70 | 107.80 | 1.658461 | -.01373 | -0.339 |
| 163   | 153.20 | 25.00 | 108.20 | 1.664615 | -.02122 | -0.531 |
| 173   | 168.80 | 25.00 | 109.00 | 1.676922 | -.03592 | -0.898 |

TABLE VII

TAYLOR-MACCOLL:  $M = 2.0039$ 

VELOCITIES AT A MISSILE TIP FROM TAYLOR-MACCOLL SOLUTION

| $\phi$ | $-v$   | $u$    | $M^*$  | $\alpha$      |               | $-\frac{v}{u}$ | $-\phi'$      |               | $\int$        |               | $\eta$        |               |
|--------|--------|--------|--------|---------------|---------------|----------------|---------------|---------------|---------------|---------------|---------------|---------------|
|        |        |        |        | $\frac{0}{2}$ | $\frac{1}{2}$ |                | $\frac{0}{2}$ | $\frac{1}{2}$ | $\frac{0}{2}$ | $\frac{1}{2}$ | $\frac{0}{2}$ | $\frac{1}{2}$ |
| 17.08  | 0      | .59700 | 1.4549 | 37            | 12            | 0              | 0             |               | 17            | 5             | 54            | 17            |
| 19.00  | .03852 | .59635 | 1.4564 | 37            | 8             | .06459         | 3             | 42            | 15            | 18            | 52            | 26            |
| 21.00  | .07538 | .59435 | 1.4600 | 36            | 56            | .12683         | 7             | 14            | 13            | 46            | 50            | 42            |
| 23.00  | .10992 | .59111 | 1.4651 | 36            | 44            | .18595         | 10            | 32            | 12            | 28            | 49            | 12            |
| 25.0   | .14283 | .58670 | 1.4715 | 36            | 26            | .24344         | 13            | 41            | 11            | 19            | 47            | 45            |
| 26.5   | .16674 | .58265 | 1.4768 | 36            | 15            | .28618         | 15            | 58            | 10            | 32            | 46            | 47            |
| 28.0   | .19017 | .57798 | 1.4829 | 35            | 56            | .32902         | 18            | 13            | 9             | 47            | 45            | 43            |
| 29.5   | .21328 | .57210 | 1.4892 | 35            | 39            | .37241         | 20            | 26            | 9             | 4             | 44            | 43            |
| 31.0   | .23626 | .56682 | 1.4966 | 35            | 20            | .41682         | 22            | 38            | 8             | 22            | 43            | 42            |
| 32.0   | .25162 | .56257 | 1.5019 | 35            | 8             | .44727         | 24            | 6             | 7             | 54            | 43            | 02            |
| 33.0   | .26713 | .55804 | 1.5078 | 34            | 51            | .47869         | 25            | 35            | 7             | 25            | 42            | 16            |
| 34.0   | .28295 | .55325 | 1.5144 | 34            | 34            | .51143         | 27            | 5             | 6             | 55            | 41            | 29            |
| 35.0   | .29938 | .54818 | 1.5222 | 34            | 14            | .54613         | 28            | 38            | 6             | 22            | 40            | 36            |
| 36.0   | .31711 | .54280 | 1.5319 | 33            | 50            | .58421         | 30            | 18            | 5             | 42            | 39            | 32            |
| 35.333 | .30596 | .54639 | 1.5260 | 34            | 05            | .55997         | 29            | 15            | 6             | 05            | 40            | 10            |

angle of shock wave

 $\phi$  = geometrical angle selected for Taylor-Maccoll solution $\phi' = \arctan$

TABLE VIII

VELOCITIES AT MISSILE TIP FROM TAYLOR-MACCOLL  
SOLUTION  $M = 3.9712$

| $\phi$ | $v^2$   | $u^2$   | $M^*$   | $\alpha$ | $-\frac{v}{u}$ | $-\phi'$ | $\int$ | $z$   |
|--------|---------|---------|---------|----------|----------------|----------|--------|-------|
| 18     | .00066  | .65448  | 1.97253 | 19 04    | .031656        | 1 49     | 16 11  | 35 15 |
| 20     | .006117 | .651540 | 1.97637 | 18 57    | .096893        | 5 32     | 14 28  | 33 25 |
| 22     | .01656  | .64571  | 1.98324 | 18 44    | .16013         | 9 05     | 12 55  | 31 39 |
| 23.5   | .02784  | .63950  | 1.99081 | 18 27    | .20865         | 11 47    | 11 43  | 30 10 |
| 25.375 |         |         |         |          |                |          |        | 30 21 |
| 19     | .00427  | .65256  | 1.97507 | 18 59    | .06475         | 3 42     | 15 18  | 34 17 |
| 21     | .01072  | .64898  | 1.97938 | 18 51    | .12853         | 7 19     | 13 41  | 32 32 |
| 23     | .02371  | .64175  | 1.98801 | 18 36    | .19221         | 10 53    | 12 07  | 30 43 |

$\phi$  = geometrical angle selected for Taylor-Maccoll solution

$\phi'$  = arctan



## BIBLIOGRAPHY

1. Liepmann, H. W., and Puckett, A. E., "Introduction to Aerodynamics of a Compressible Fluid", John Wiley & Sons, 1947
2. Puckett, A. E., "Supersonic Nozzle Design for Engineers", May, 1946
3. Heybe, "The Prandtl-Busemann Method for the Graphical Evaluation of Two-dimensional Supersonic Flow, its Application to the Design of a Wind Tunnel Nozzle and the Appropriate Corrections", Kochel Report 55/56, February 4, 1941.
4. Sauer, R., "Theoretische Einführung in die Gasdynamik", Berlin Springer, 1943
5. Poritsky, H., & others, "Sauer's Graphical Numerical Method for Supersonic Axially Symmetric Flows and its Application to Pressure Distribution on Boat Tail Shapes." General Electric Report #45777, June 26, 1946
6. Taylor, G. I. and Maccoll, J. W., "Air Pressure on a Cone Moving at High Speeds", Proceedings of the Royal Society, Vol. 139, pp 278-311. 1933
7. Durand, W. F., Aerodynamic Theory, Volume III, Durand Reprint, 1943
8. Chien, W. Z., "Wave Drag of a Projectile Nose at a Supersonic Velocity by the Karman-Moore Method." ORDCIT, Report #4-24, April 19, 1946

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